



On the Design and Placement of a Supplementary Damping Controller in an Embedded VSC-MTDC Network

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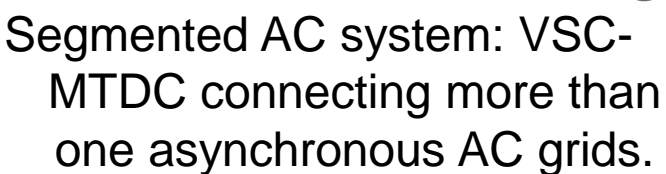
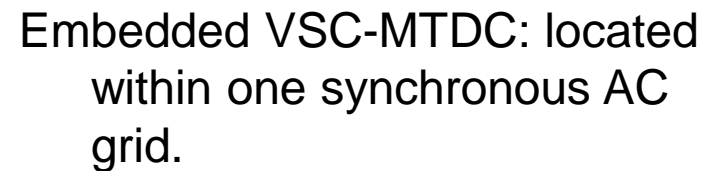
Presented by:

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Presentation Outline

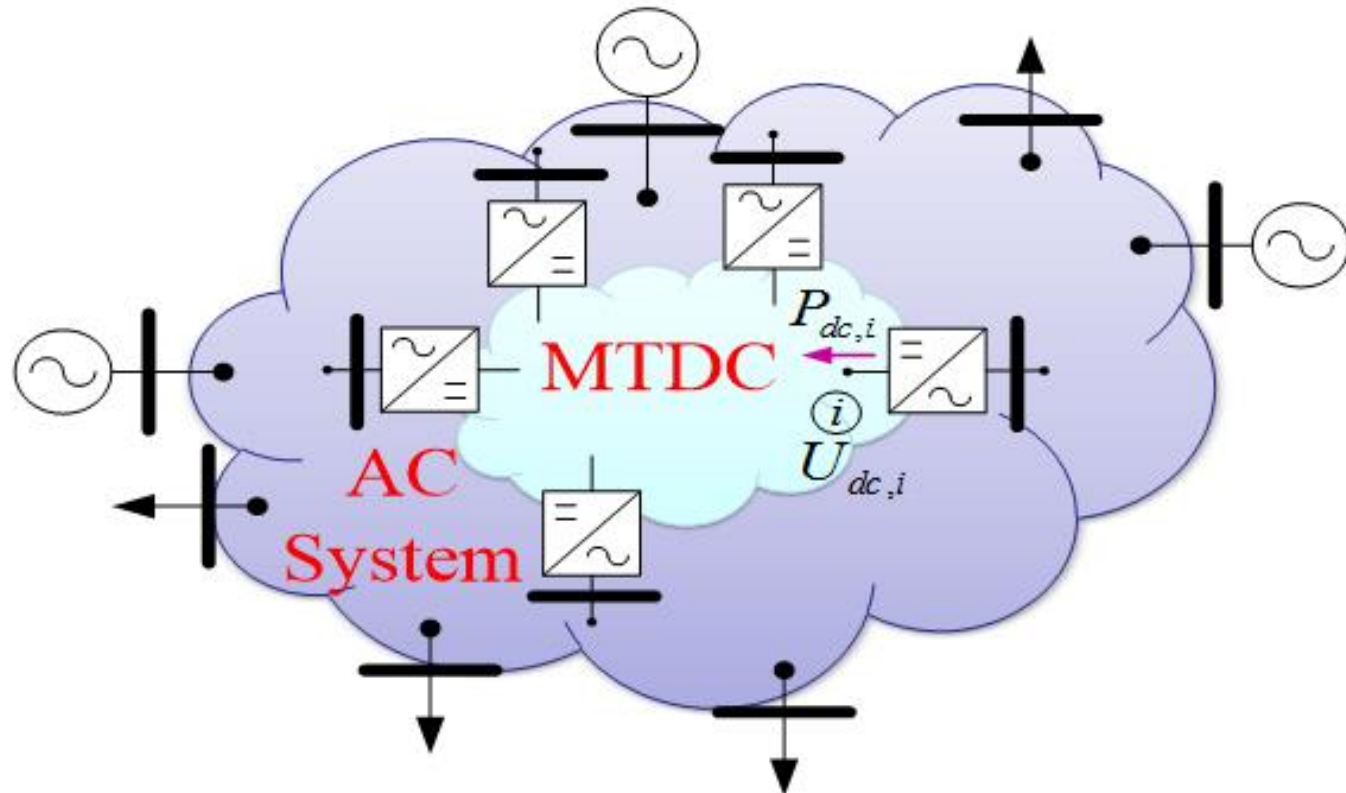
- Introduction
- Motivation
- Power System Model
- Controller Design
- Conclusions



Introduction: Embedded VSC-MTDC Network

AC/DC Power System Model:

- One slack bus
- VSC represented by average model
- Master-slave DC voltage control



Introduction: Embedded VSC-MTDC Network

MTDC Control Imperatives in AC/DC Power System

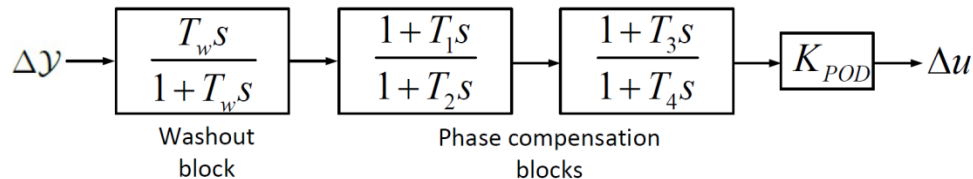
- **Primary control:** active&reactive power, DC voltage, AC voltage
- **Supplementary control:** Power Oscillation Damping (POD), frequency support
- **Control coordination:** PSS, other FACTS POD

Motivation

- ❑ Supplementary (POD) control not sufficiently investigated as compared to primary control in VSC-MTDC
- ❑ Multiple damping controllers: adverse control interactions
- ❑ Control coordination problem through nonlinear optimization:
 - Complex objective functions
 - Time-consuming solutions
- ❑ Strategic placement of supplementary controller(s)

Motivation

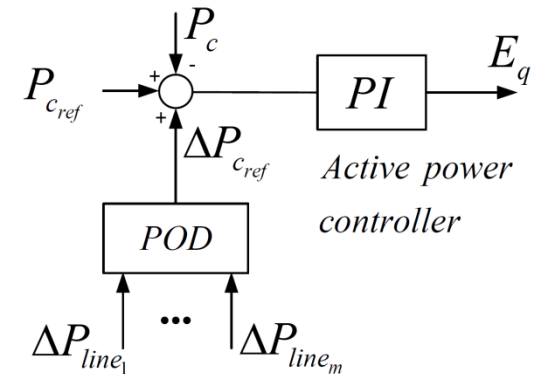
- MLQG-MISO control allows damping of targeted modes of interest, other modes are not affected



SISO control structure

Assumptions:

- Negligible time delays
- PMUs readily available



MISO control structure

Power System Model

- Nonlinear DAE system model:

$$\dot{x} = f(x, y, u)$$

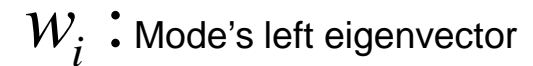
$$0 = g(x, y, u)$$

- Linearized system model:

$$\Delta \dot{x} = f_x \Delta x + f_y \Delta y + f_u \Delta u$$

$$0 = g_x \Delta x + g_y \Delta y + g_u \Delta u$$

Linearization conducted around the equilibrium point of the DAE system.

 \mathbf{v}_i : Mode's right eigenvector
$$\frac{\partial \lambda_i}{\partial q} = R_i \frac{\partial F(s, q)}{\partial q} \Big|_{s=\lambda_i} = w_i^T B \frac{1}{(1 - F(\lambda_i, q))^2} C v_i$$

Power System Model

- Linearized state-space system model:

$$\dot{x} = Ax + Bu + \Gamma w$$

$$y = Cx + v$$

w : Process noise

v : measurement noise

- Modal variables:

$$z(t) = Mx(t)$$

MLQG Control Design

- Cost function:

$$J_k = \lim_{T \rightarrow \infty} E \left\{ \int_0^T \left(x^T (M^T Q_m M) x + u^T R u \right) dt \right\}$$

Q_m : Weighting matrix for modal variables

R : Weighting matrix for controller output

M : Mapping matrix

Feedback control law given by: $u(t) = -K\hat{x}(t)$

K : MLQG controller gain

MLQG Control Design

$\hat{x}(t)$ obtained using Kalman filter: $\dot{\hat{x}}(t) = A\hat{x} + Bu + L(y - C\hat{x}) + Lv$

L : Constant estimation error feedback matrix, obtained by the solution of Algebraic Riccati Equation (ARE):

$$\dot{\hat{x}}(t) = A\hat{x} + Bu + L(y - C\hat{x}) + Lv$$

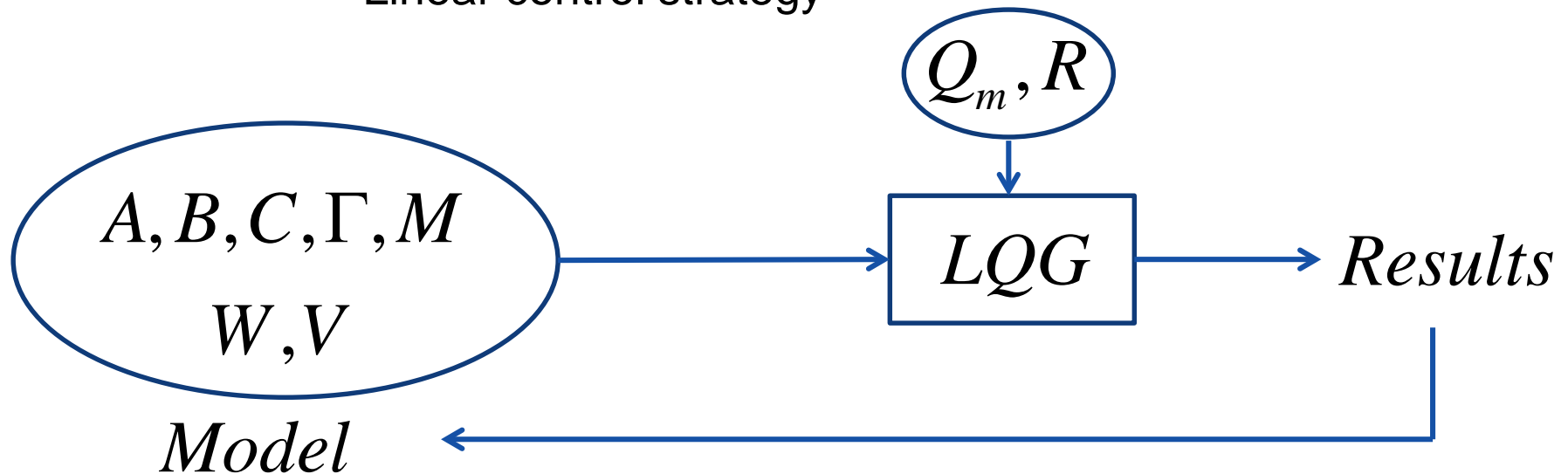
ARE solution is according to cost function for Kalman filter:

$$J_L = \lim_{T \rightarrow \infty} E \left\{ \int_0^T (x^T W x + u^T V u) dt \right\}$$

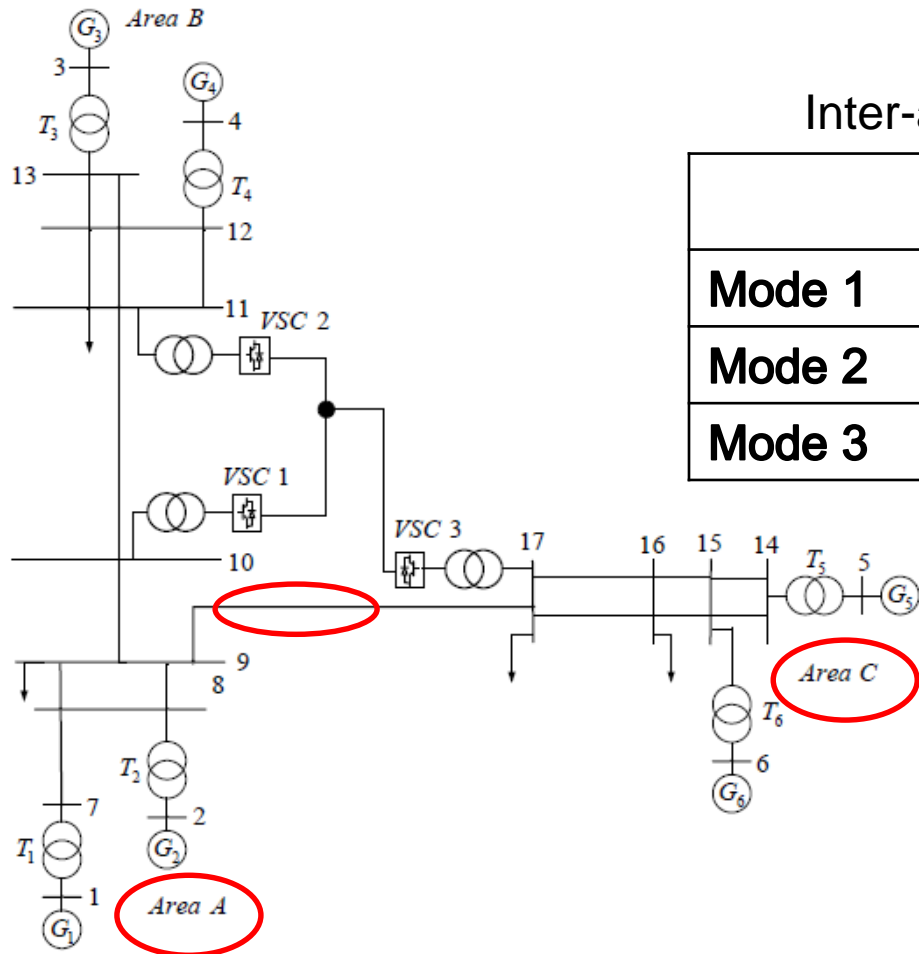
MLQG Control Design

MLQG POD supplementary controller design merits:

- Enhanced robustness
- Targeted damping of specific oscillatory modes (weighting matrices)
- Linear control strategy



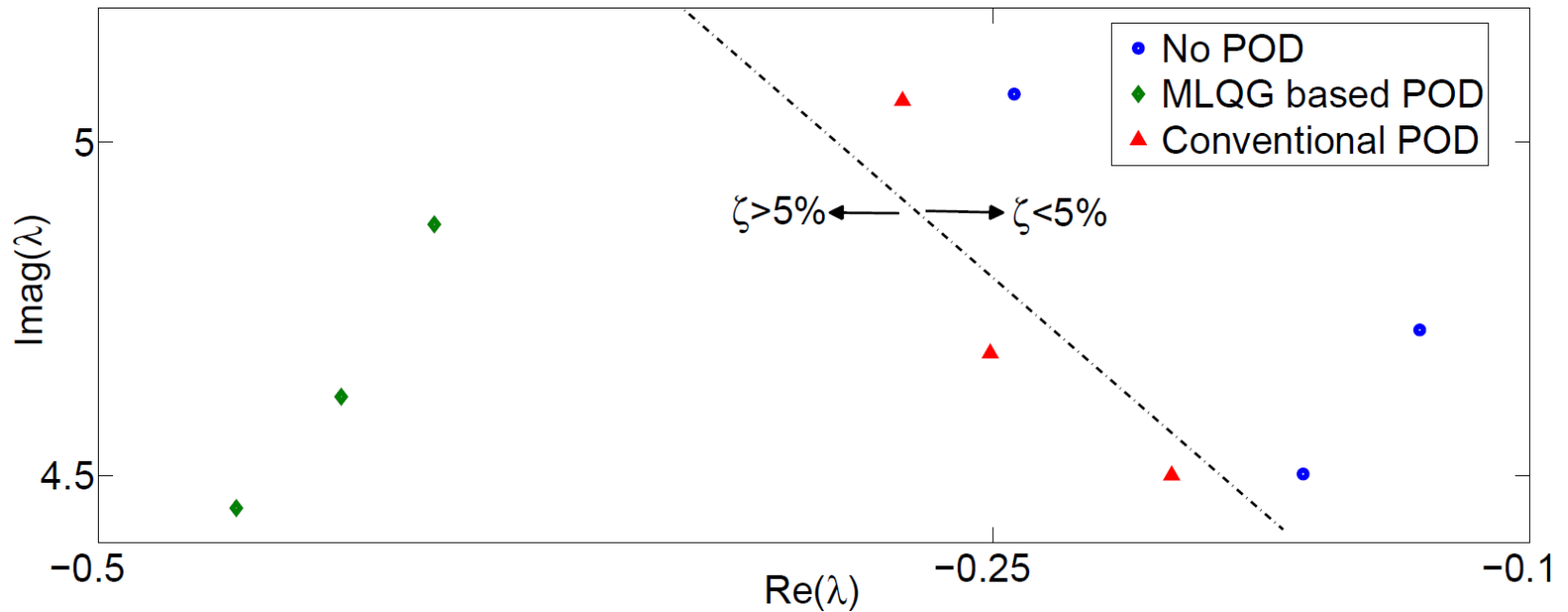
Results



Inter-area modes' observabilities (normalized).

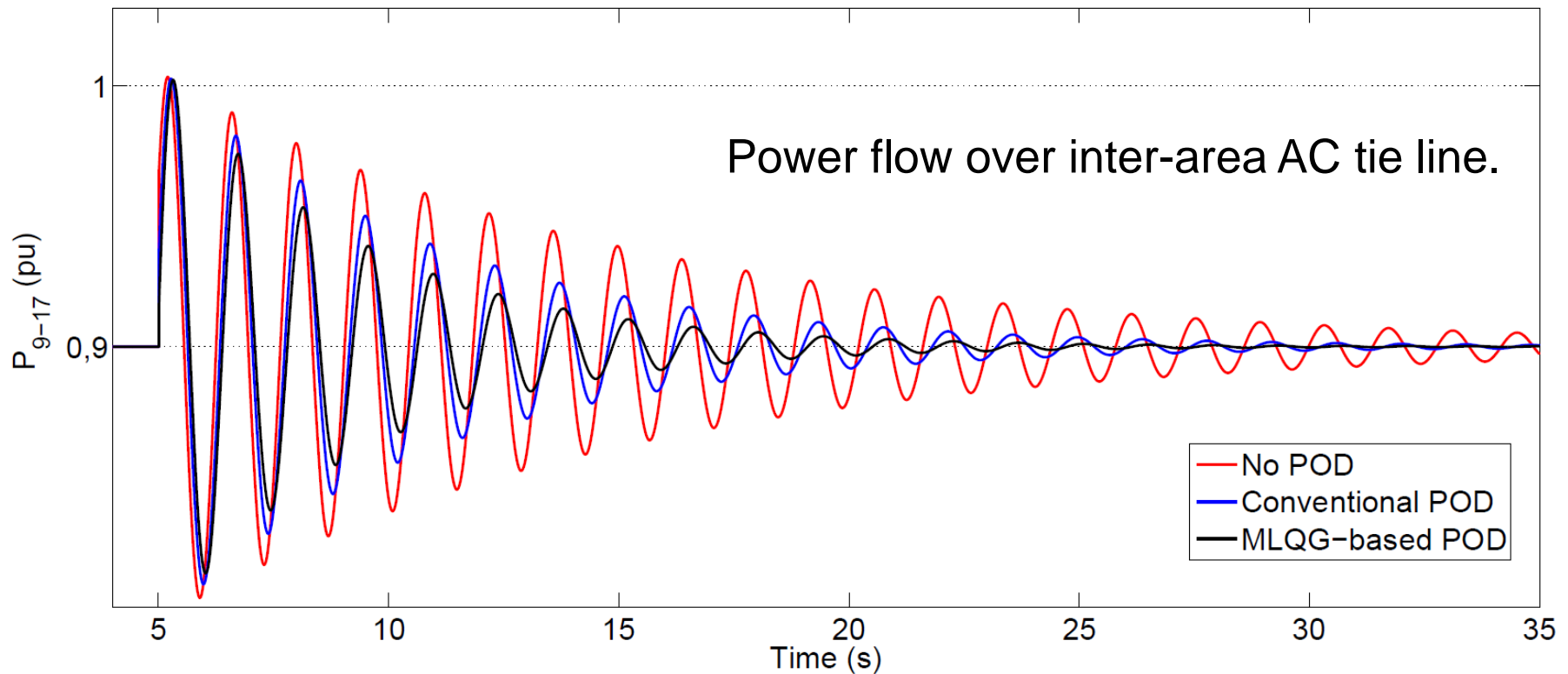
	P₁₂₋₁₃	P₅₋₁₄	P₁₁₋₁₂
Mode 1	1	0.4027	0.6974
Mode 2	0.3282	1	0.3402
Mode 3	0.6813	0.3661	1

Results



Inter-area modes' locations in complex plane.

Results



Disturbance: 10% load increase for 100 ms.

Conclusions & Future Work

- ❑ Research theme: AC/DC power system stability enhancement & control through MTDC supplementary controls
- ❑ Strategic positioning of a single damping controller within an embedded VSC-MTDC network
- ❑ Investigation of supplementary (POD) control in case of droop control used for DC voltage regulation.

Thank you! Questions?