

Corrosion of FeCr alloys in Solid Oxide Fuel Cells

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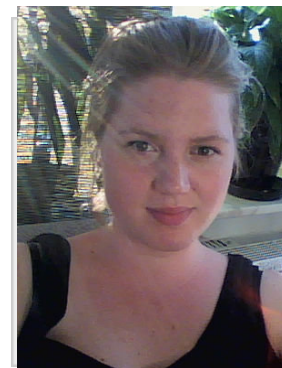
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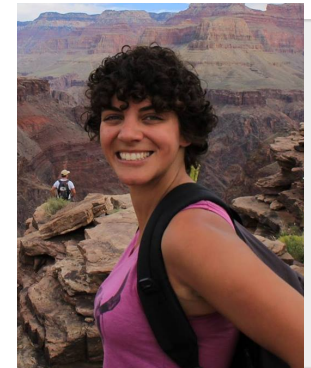
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Falk Windisch



Jan
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Claudia
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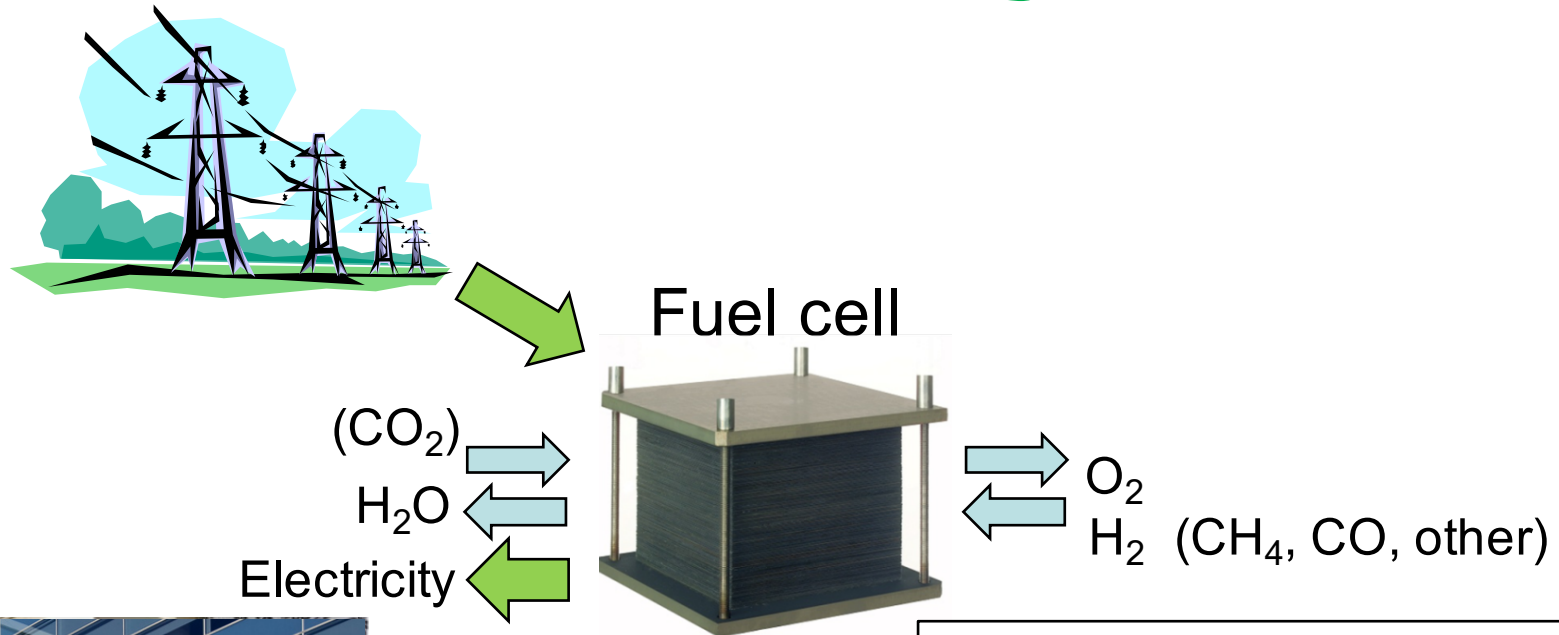
Project partners



CHALMERS



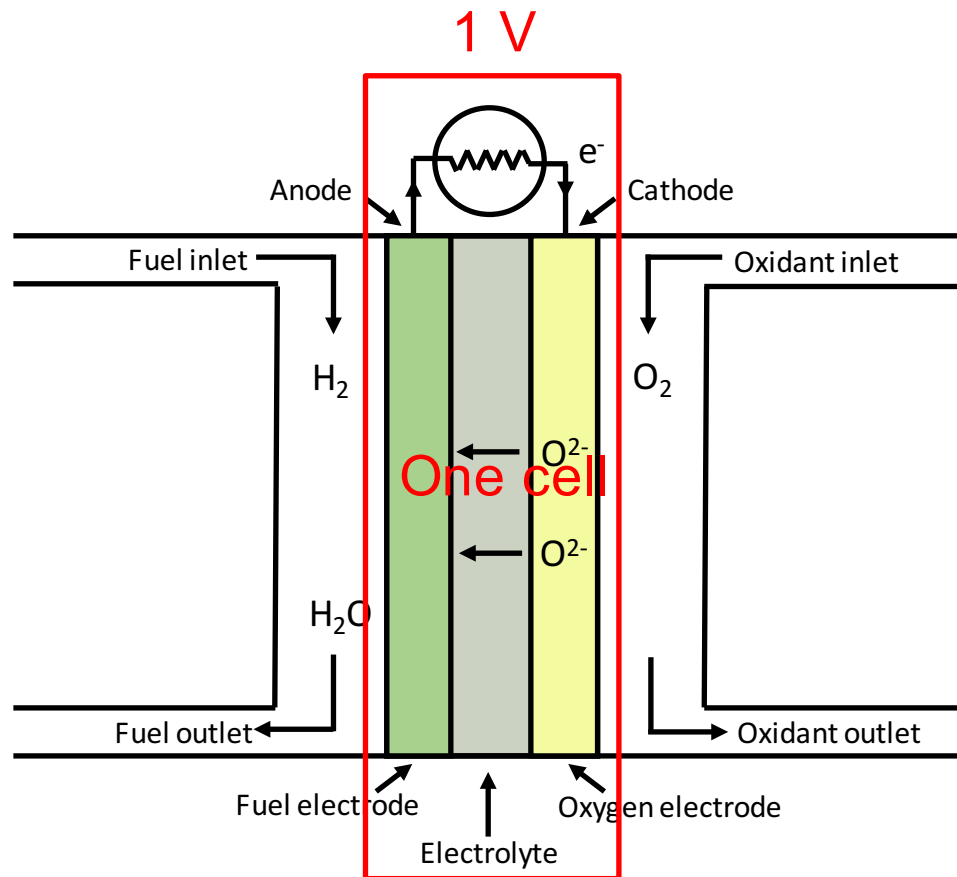
Solid Oxide Fuel Cells



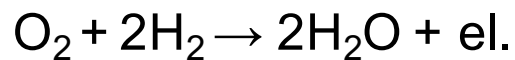
Truck or RV
Auxiliary Power
Units (APUs)
(CHP)

- Efficient power generation (60 el%)
- Fuel flexible
- Low emissions
- Scalable

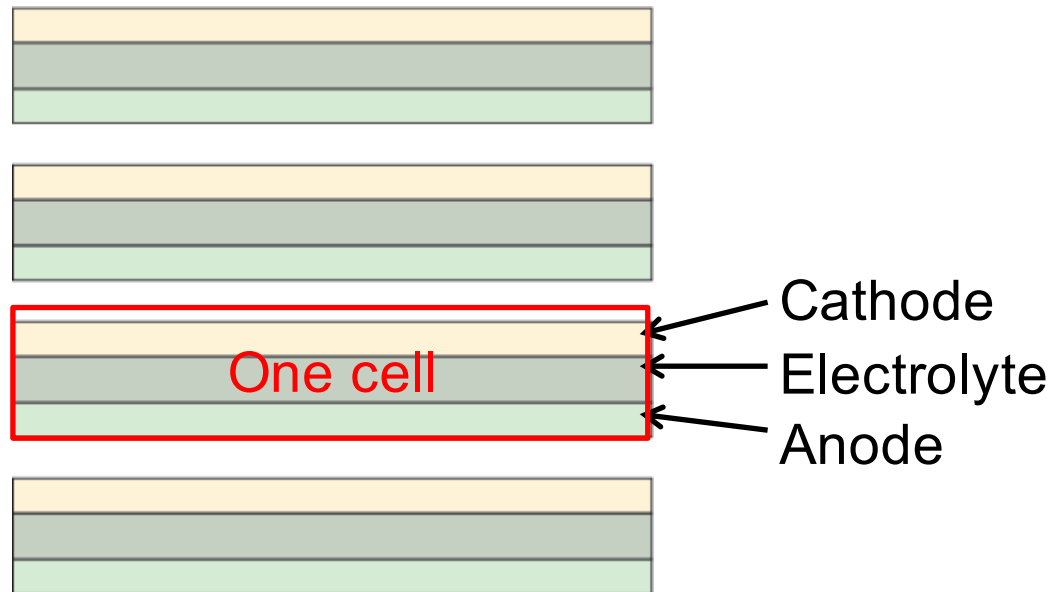
Solid Oxide Fuel Cell



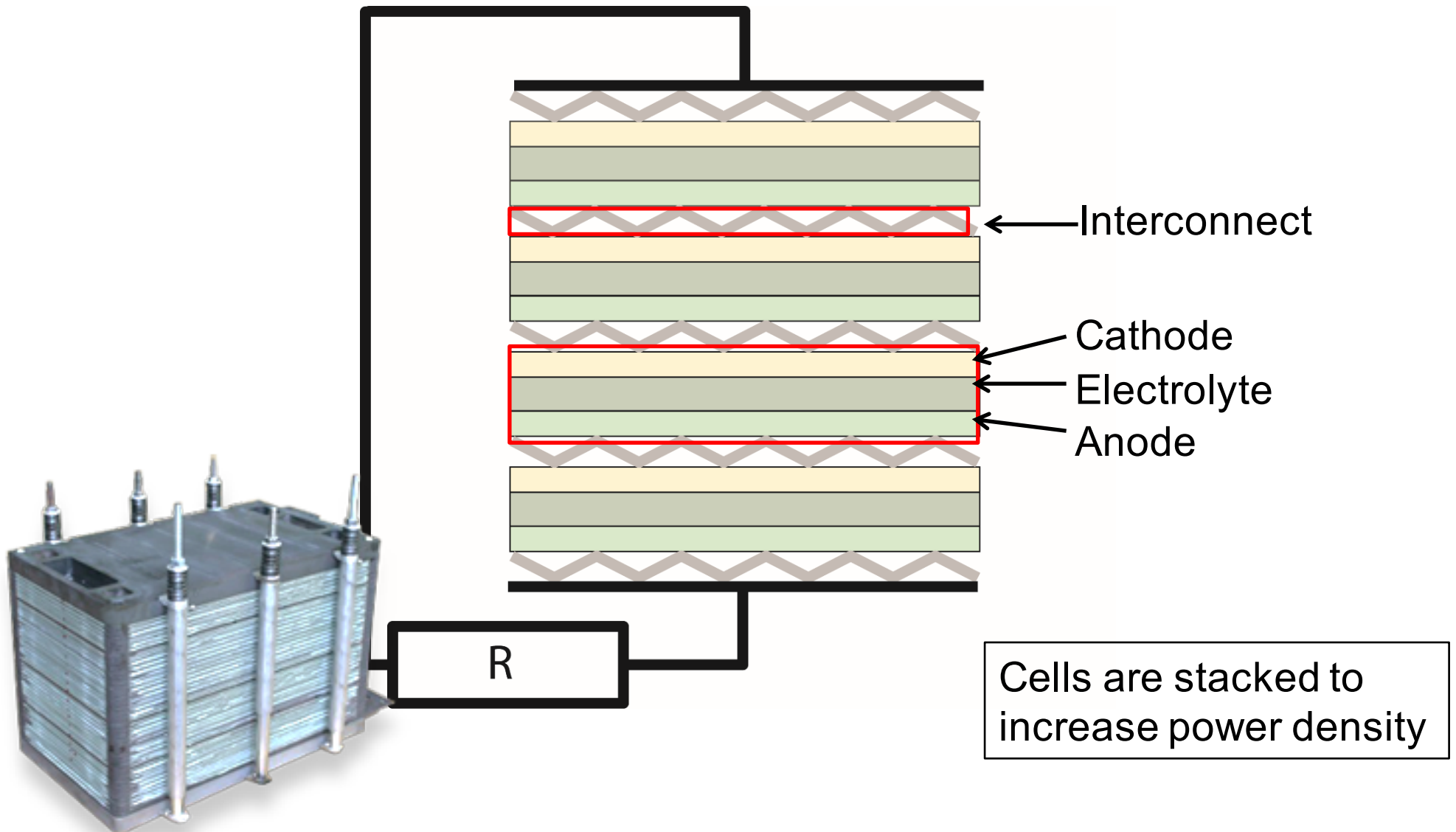
- Operating temperature: 500 – 900 °C
- Controlled reaction of hydrogen and oxygen
- Various fuels can be used
- Ceramic components

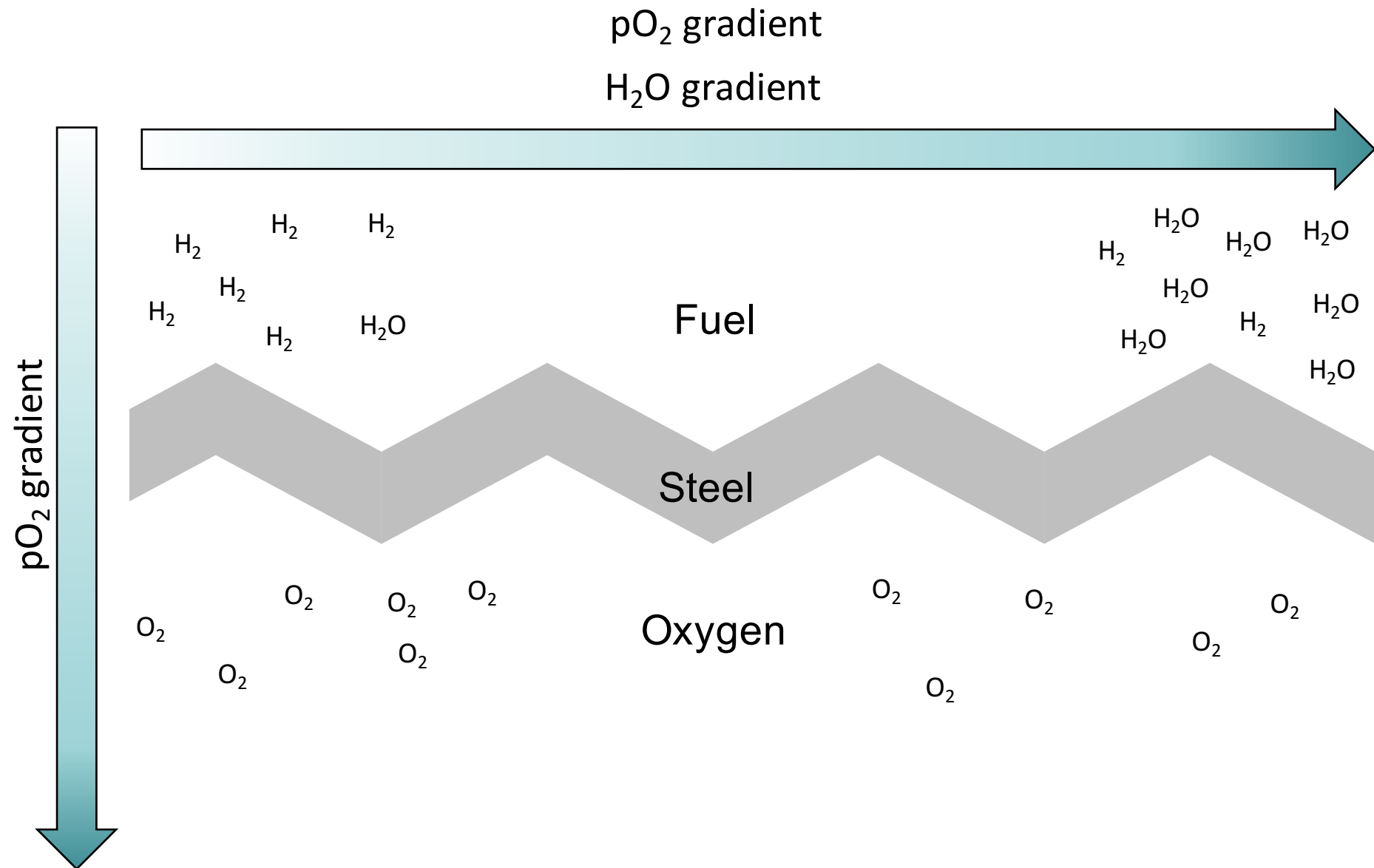


Stacking of cells



Stacking of cells





Sustainable = economically viable?

SOFC technology faces two major challenges:

Cost



Degradation



-Steel interconnects

Commercialization of SOFC

Material challenges for metallic SOFC interconnects

- Corrosion
- Chromium evaporation
- Degradation of electronic conductivity



Precoated steel concept

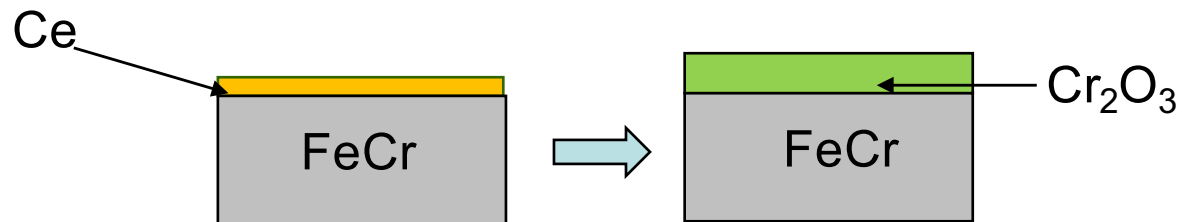


- PVD coatings
- Roll to Roll process
- Production line
- High capacity
- 800mm width
- Multilayered coatings



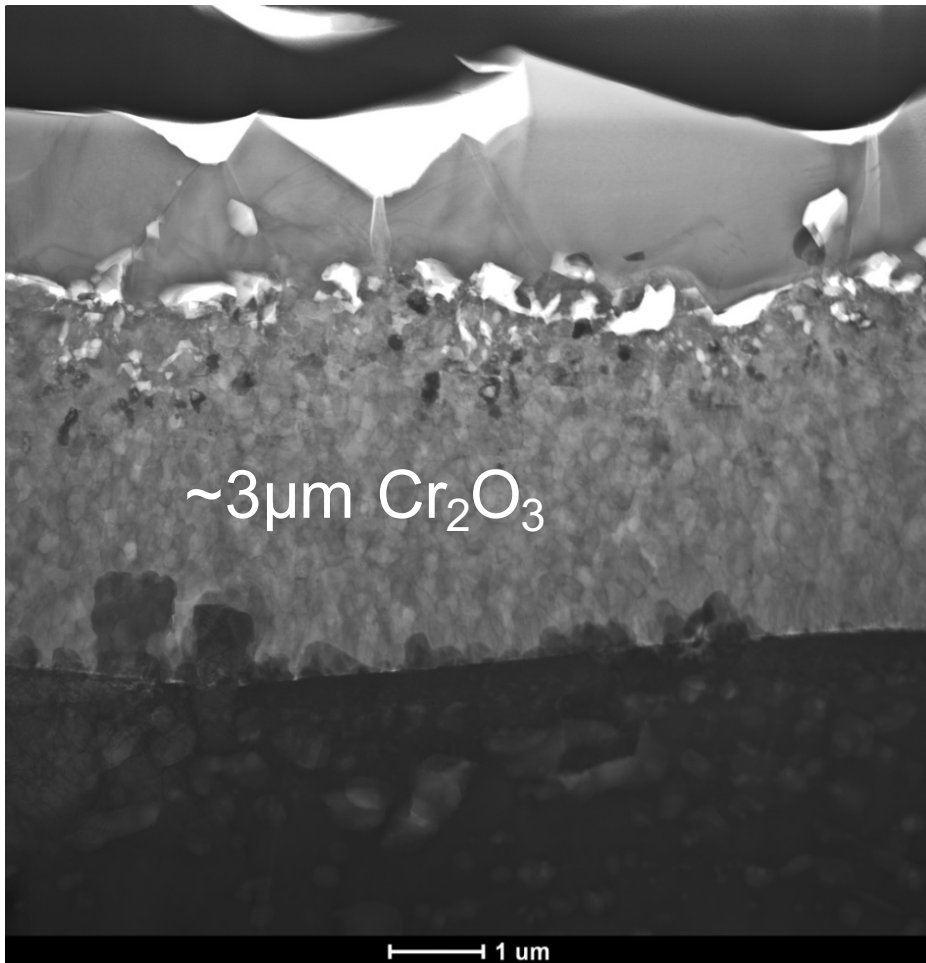
Solving corrosion

- Adding reactive element coating by PVD
 - Promotes chromia formation
 - Decreases oxidation speed



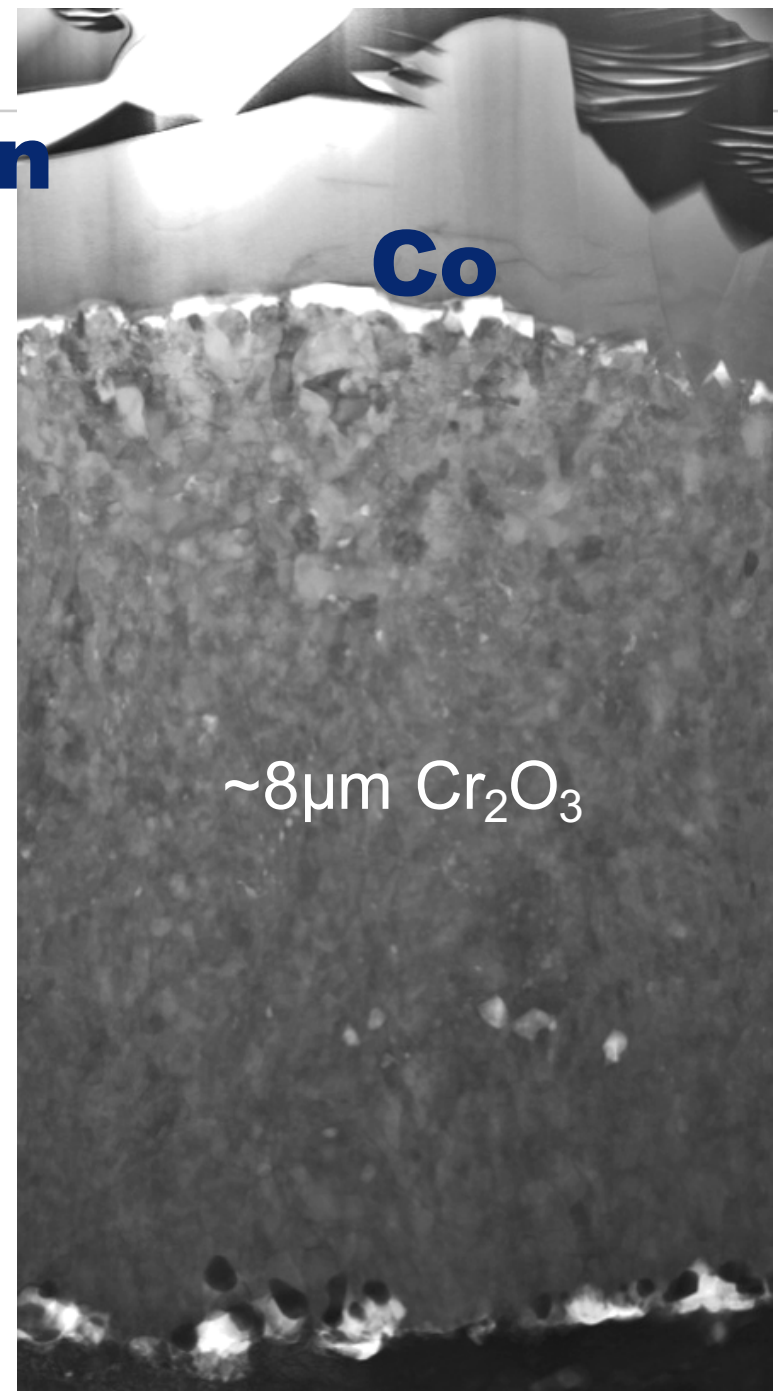
Comparison

Co/Ce



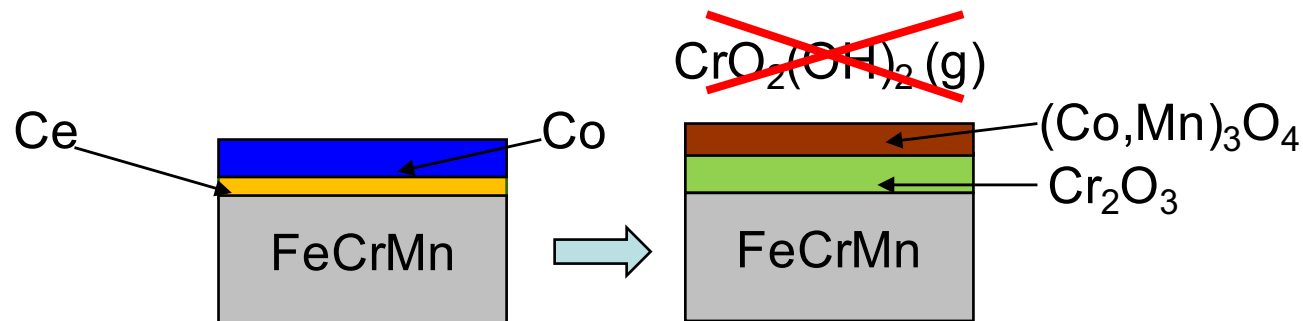
Ce slows down the growth of the Cr₂O₃ layer

Co

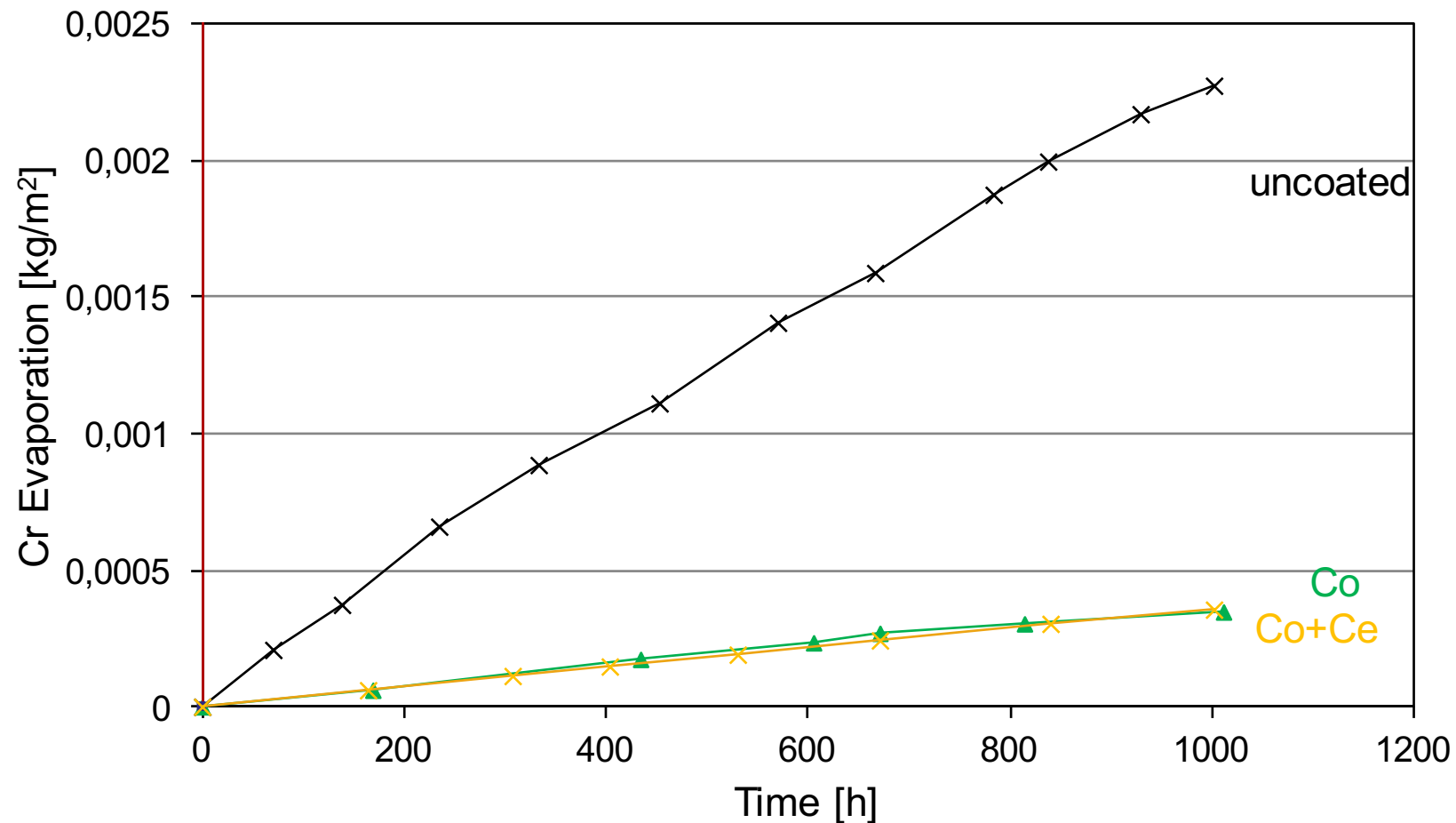


Solving chromium evaporation

- Adding metallic Co coating by PVD
 - Oxidizes to Co-Mn-spinel
 - Low Cr activity

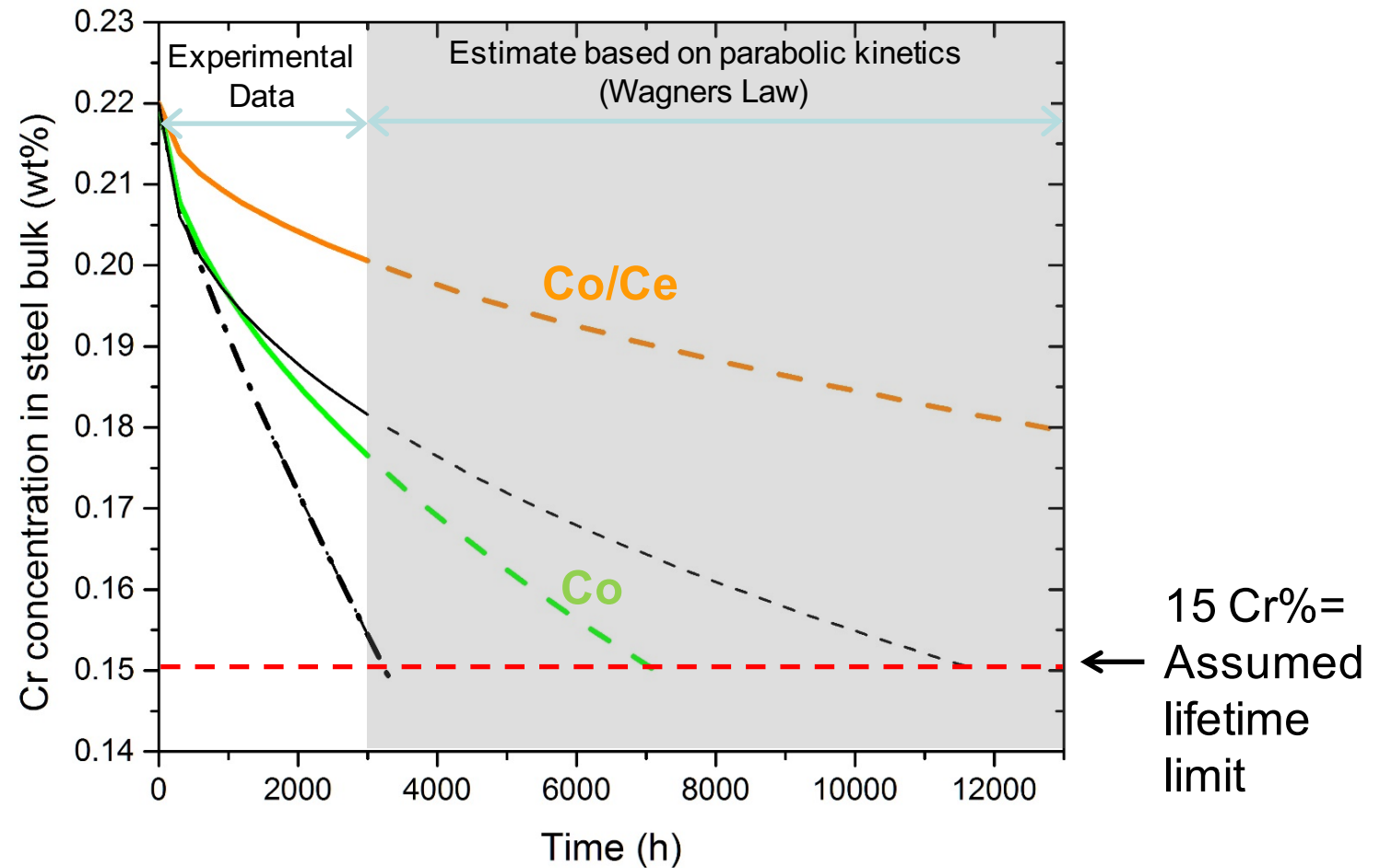


Cr Evaporation (850°C in air + 3% H₂O)



Co+Ce coating as good as Co coating

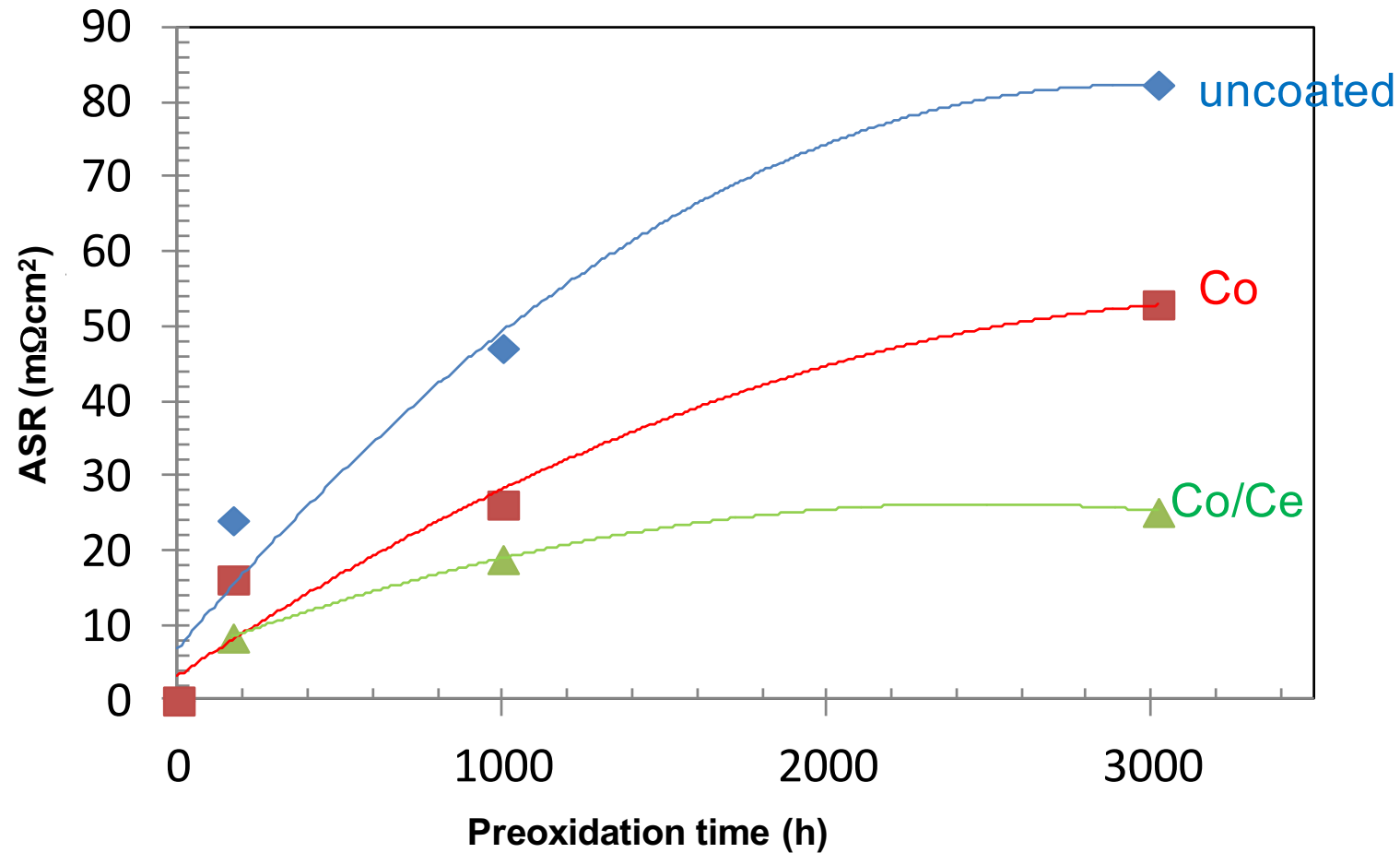
Lifetime estimate - Calculated remaining Cr





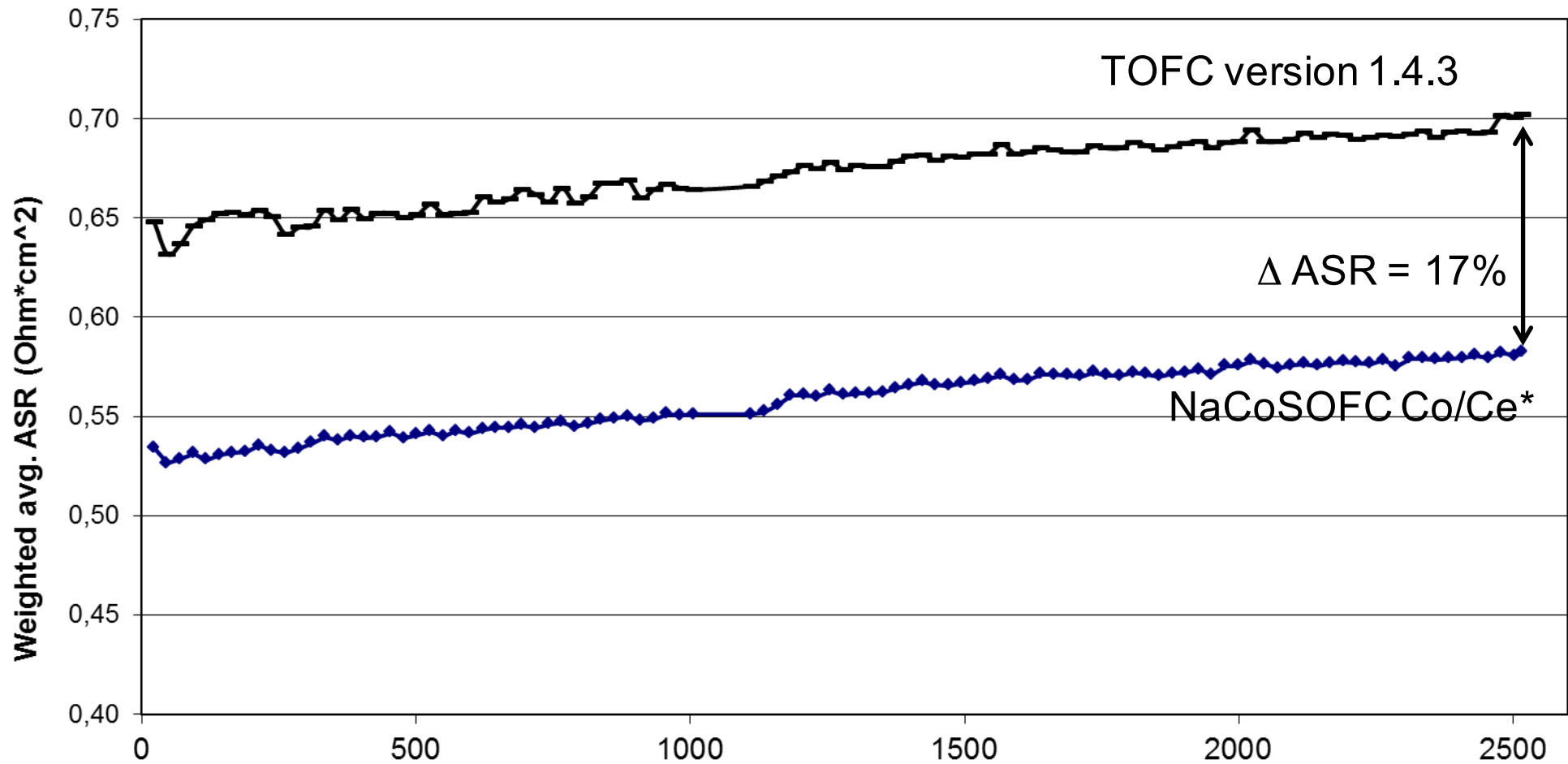
ASR characterization

@ Department of Chemistry, University of Oslo FERMiO

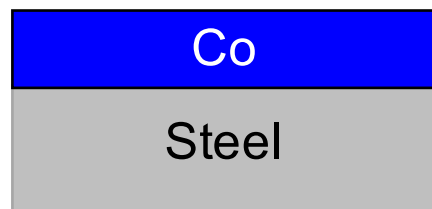


2500h Stack Test

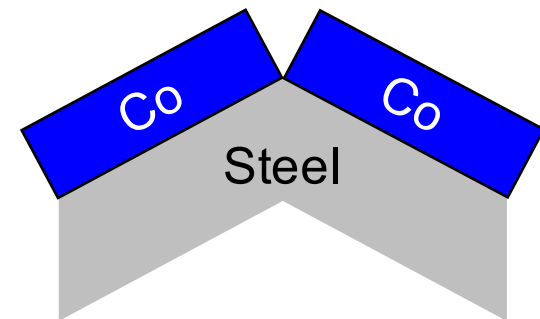
@ 700°C, 20A



Effect of deformation



Interconnect forming

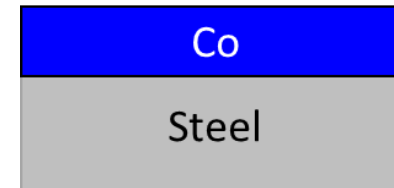


Increased Cr
vaporization?

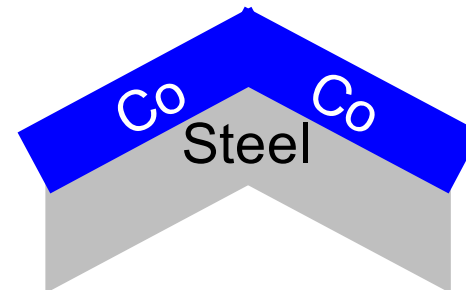
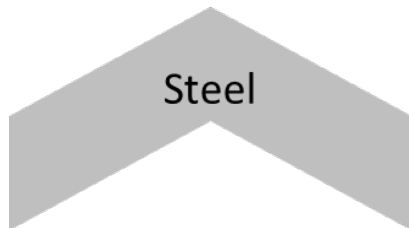
Materials investigated



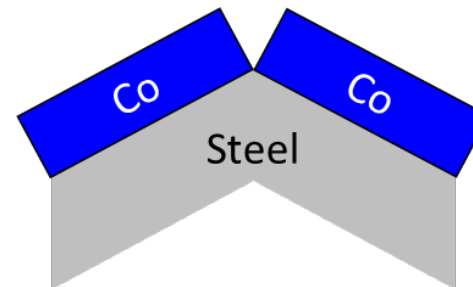
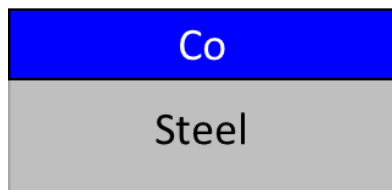
Reference:
Uncoated



Reference:
Coated

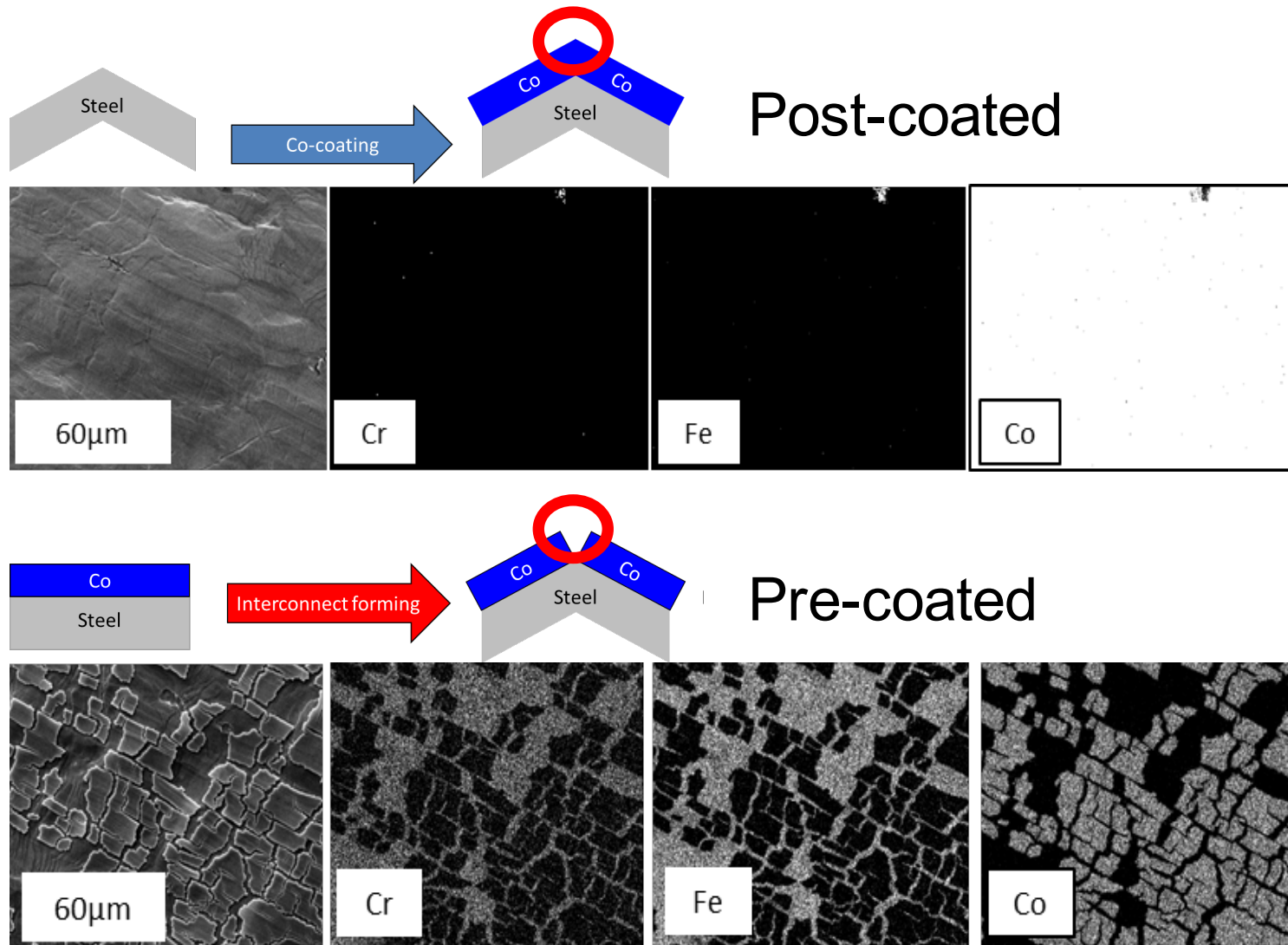


Post-
coated



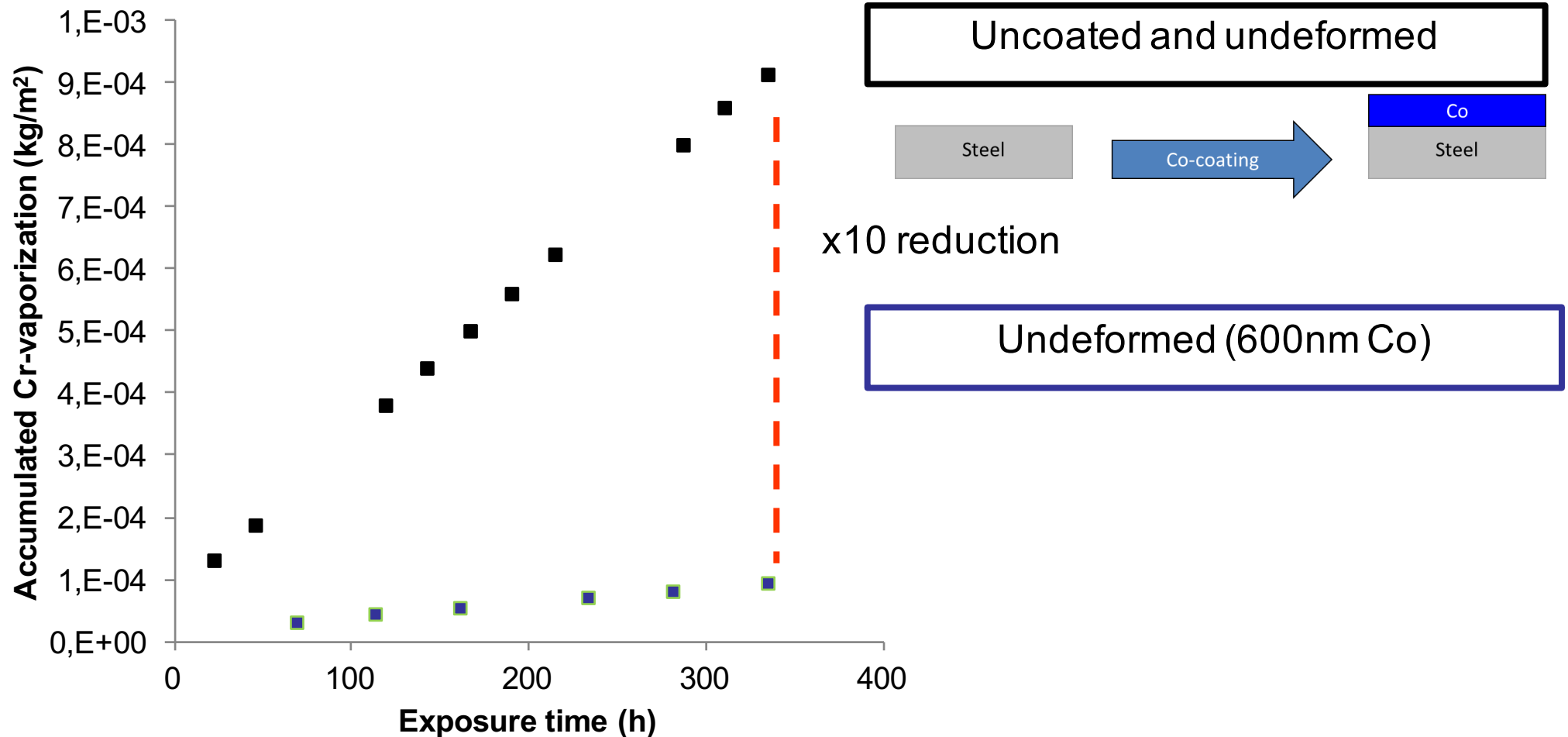
Pre-
coated

Before exposure



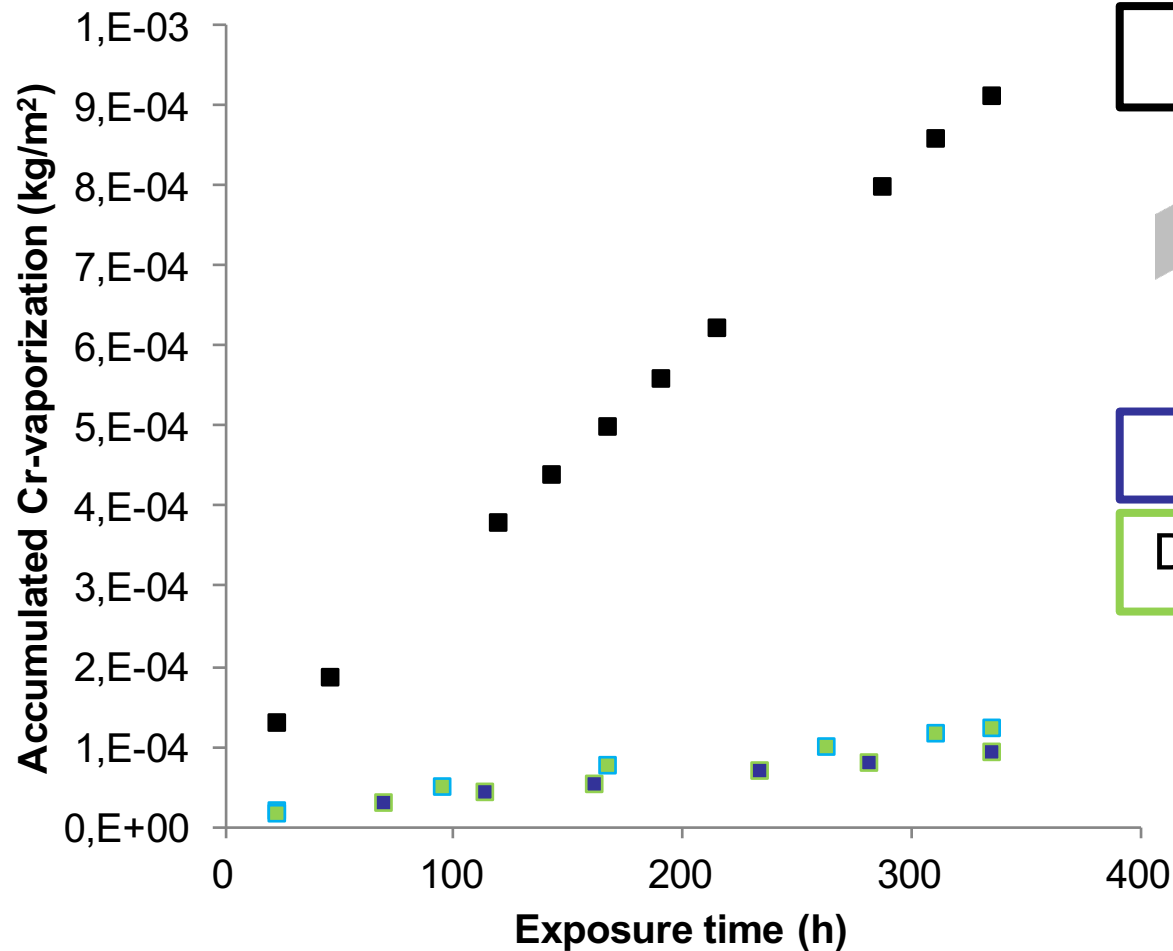
Cr vaporization

Air, 850 °C

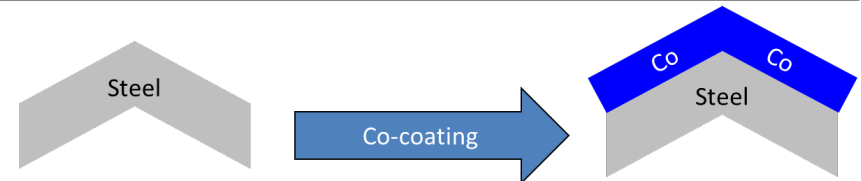


Cr vaporization

Air, 850 °C



Uncoated and undeformed

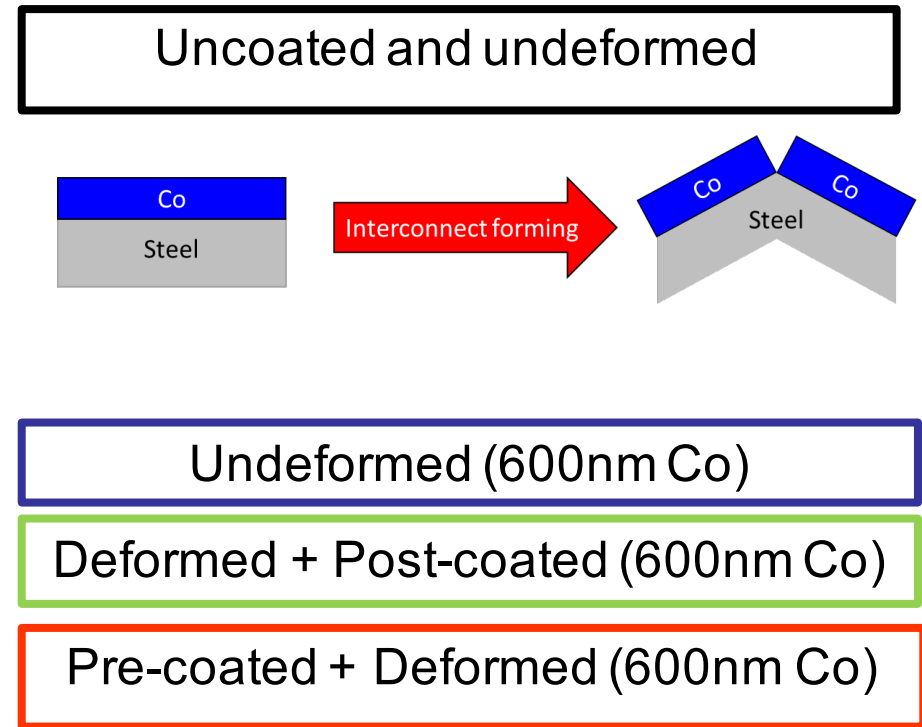
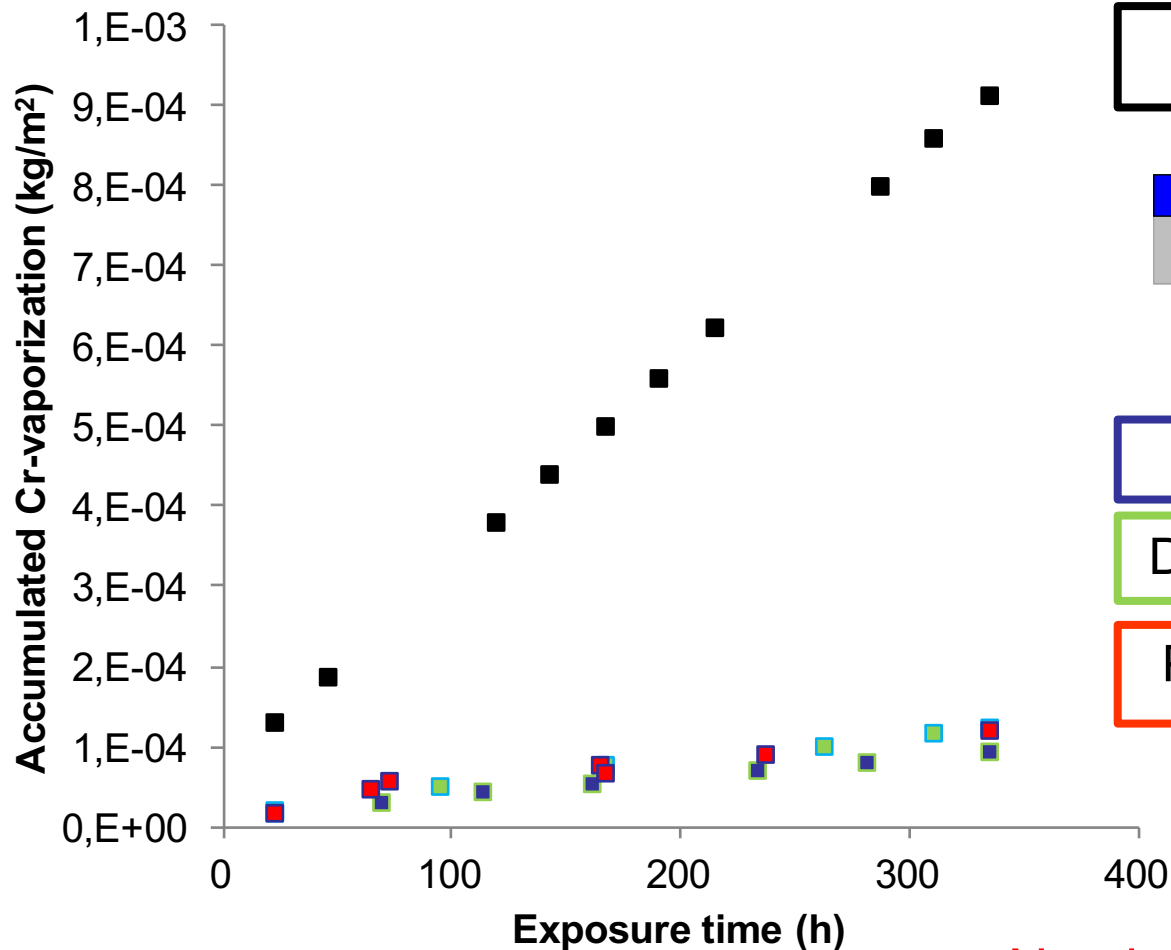


Undeformed (600nm Co)

Deformed + post-coated (600nm Co)

Cr vaporization

Air, 850 °C



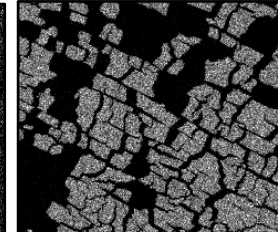
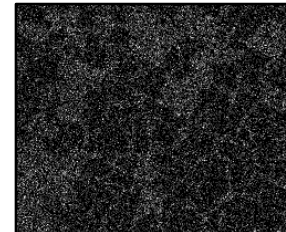
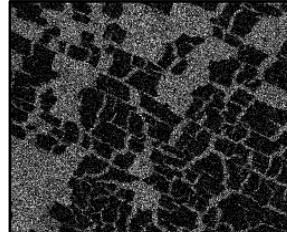
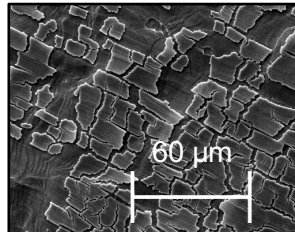
No signs of increased Cr-vaporization
after mechanical deformation/stamping

Cr

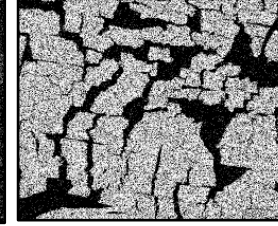
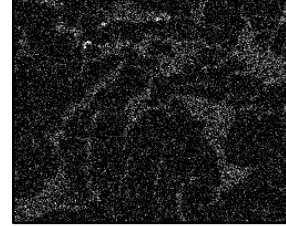
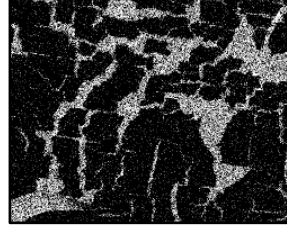
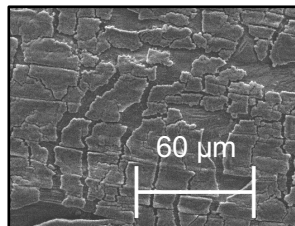
Mn

Co

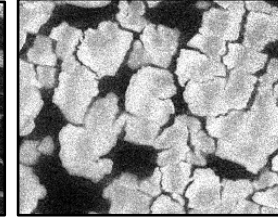
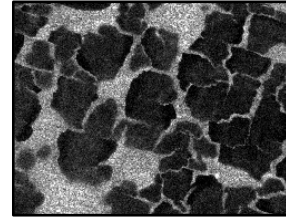
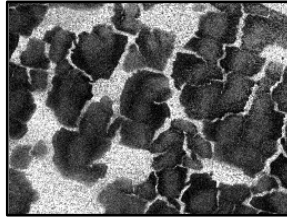
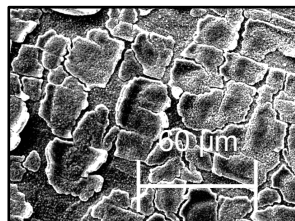
Unexposed:



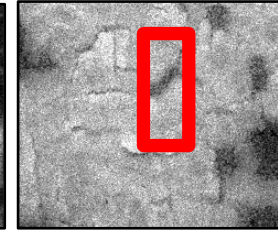
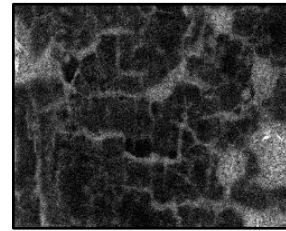
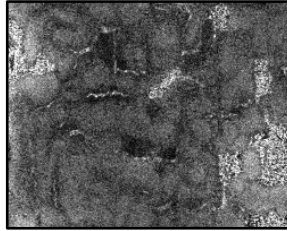
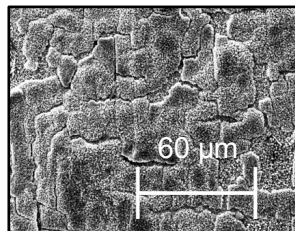
6 minutes:



8 hours:



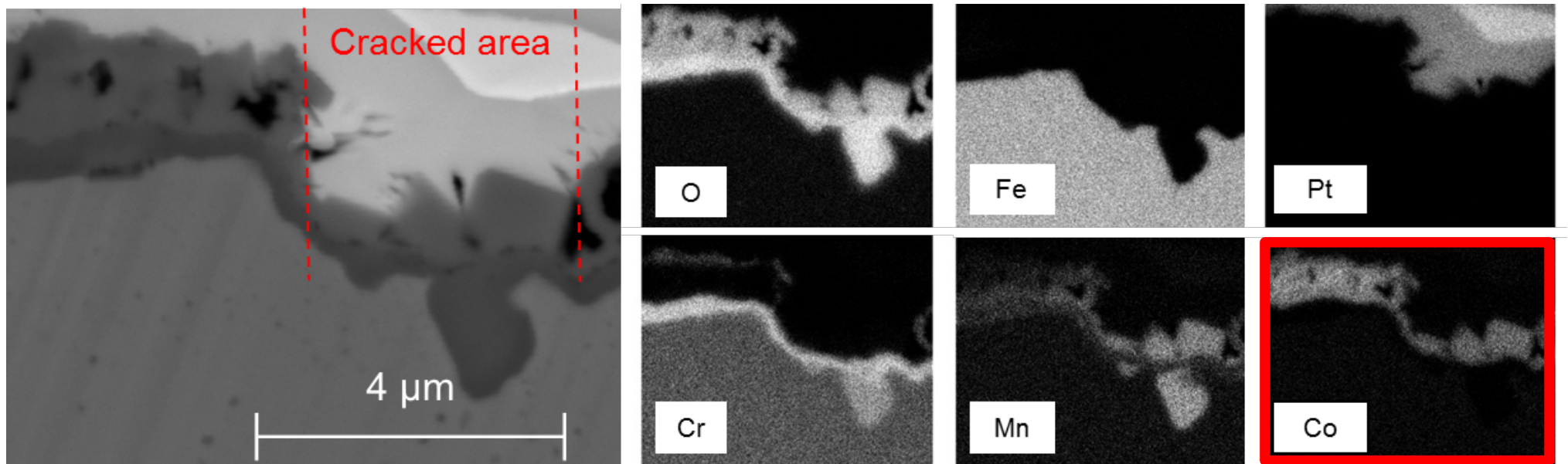
24 hours:



Mn enrichment within the cracked area

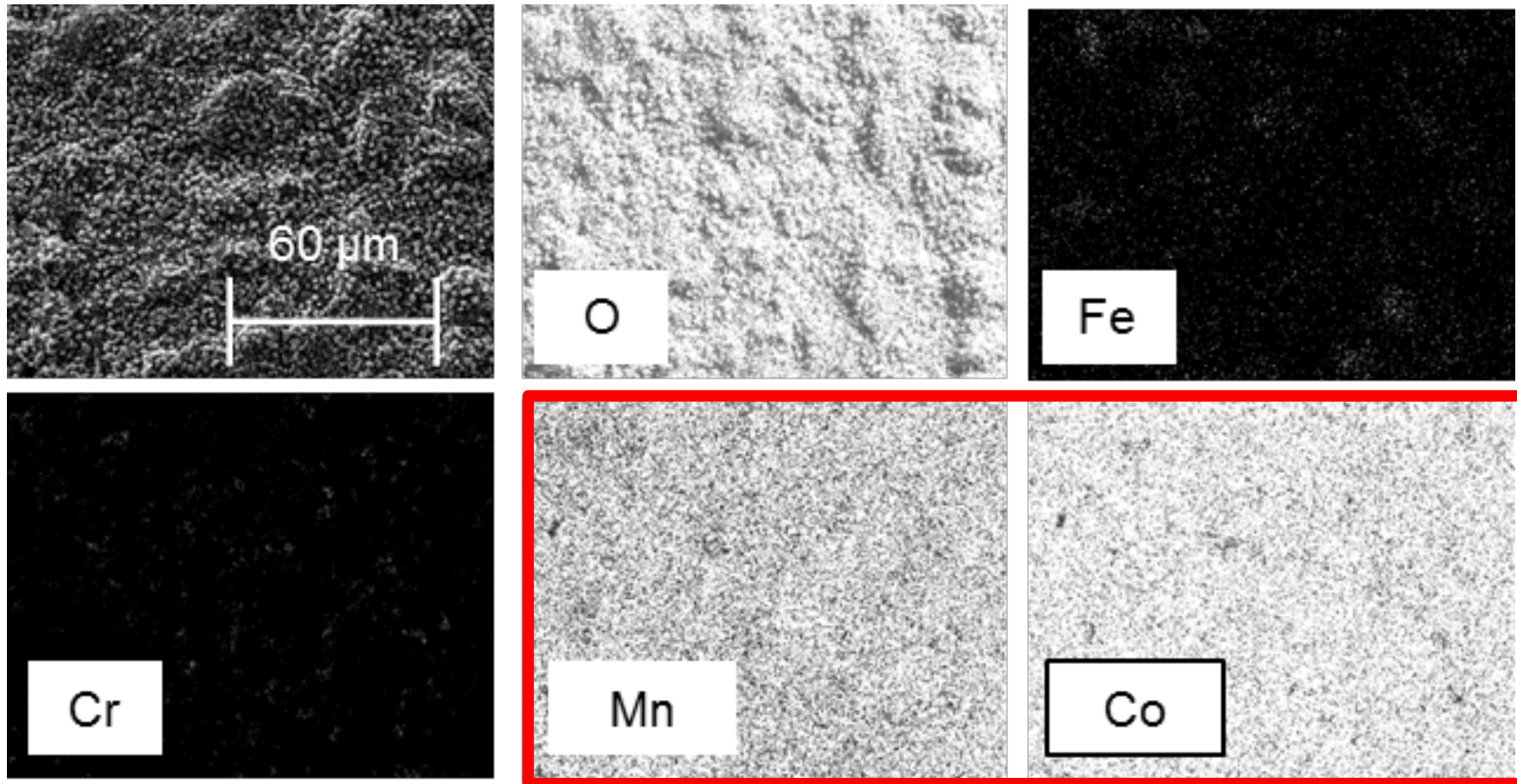
More homogenous Cr, Mn and Co signal after 24 h

24 h (Air, 850 °C):



Thin Co-rich layer within the cracked area
Growth of $(\text{Co,Mn})_3\text{O}_4$ crystals within cracked area

336 h (Air, 850 °C):



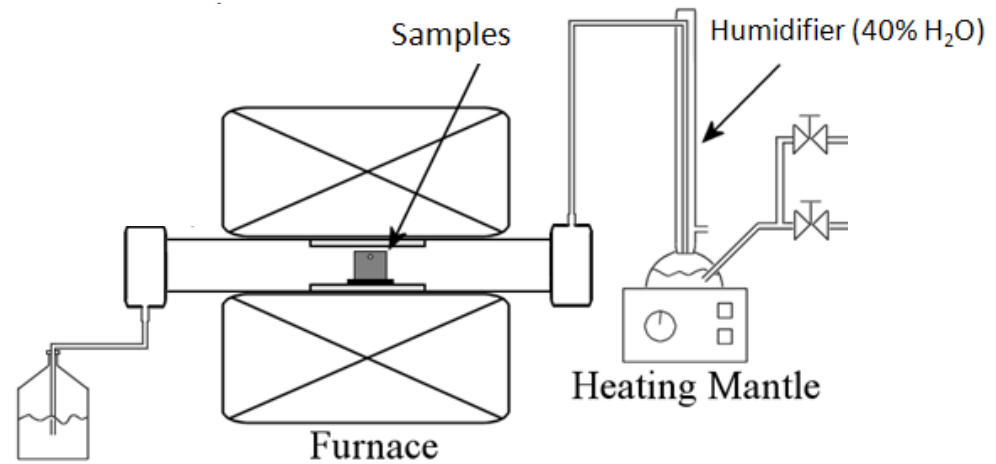
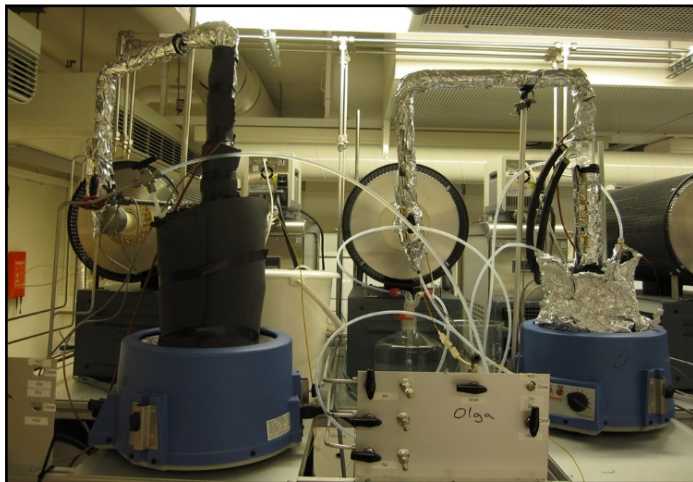
Surface homogenously covered by an oxide rich in Co and Mn

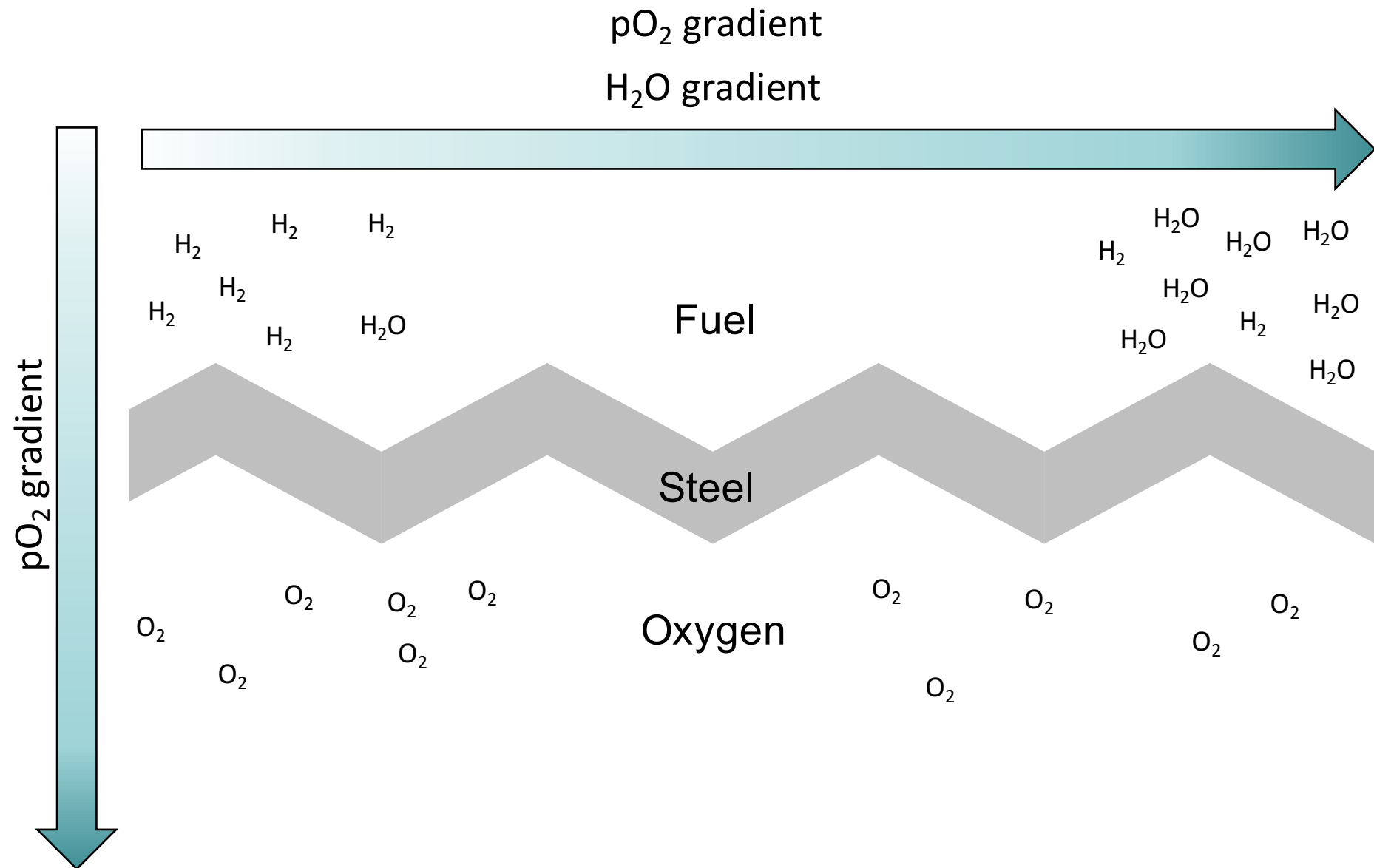
Fuel side exposures

Temperature: 850 °C

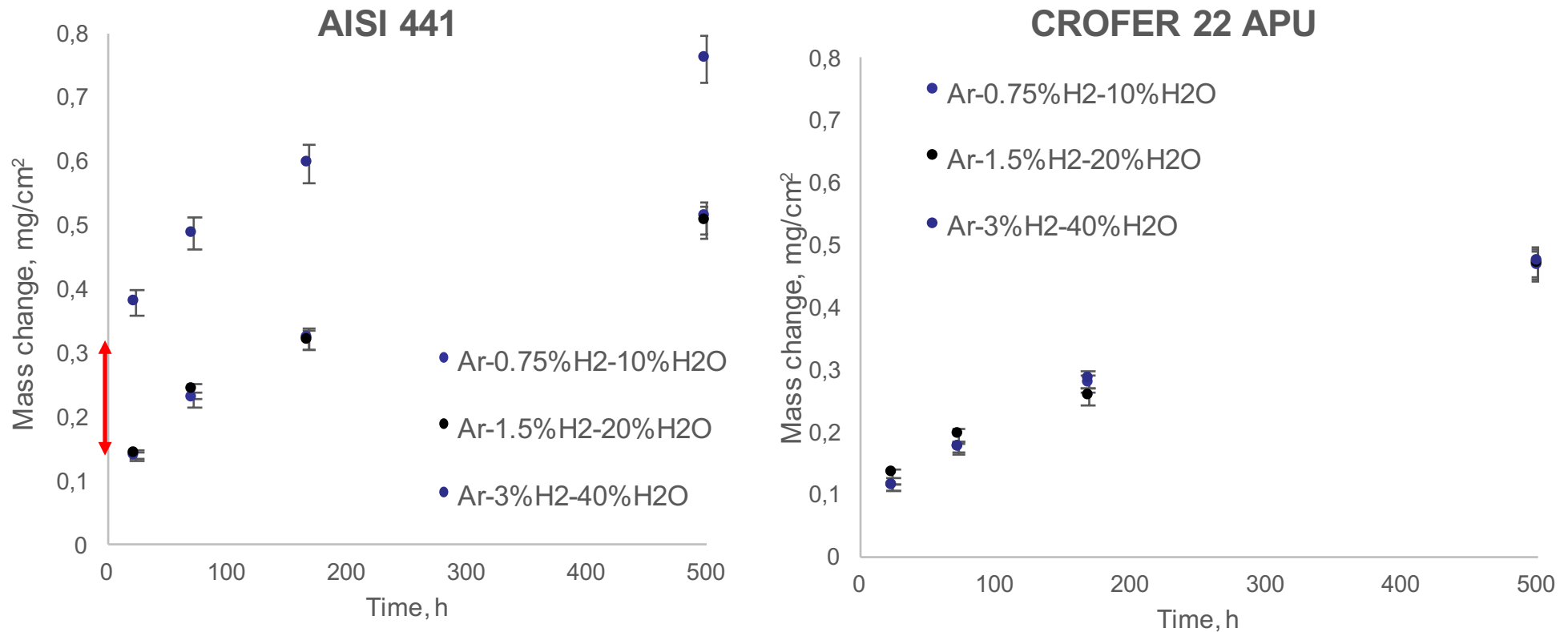
Atmosphere: Ar – 3% H₂ – 40% H₂O: $pO_2 = 10^{-15}$

Sample size: 15 x 15 x 0.2 mm

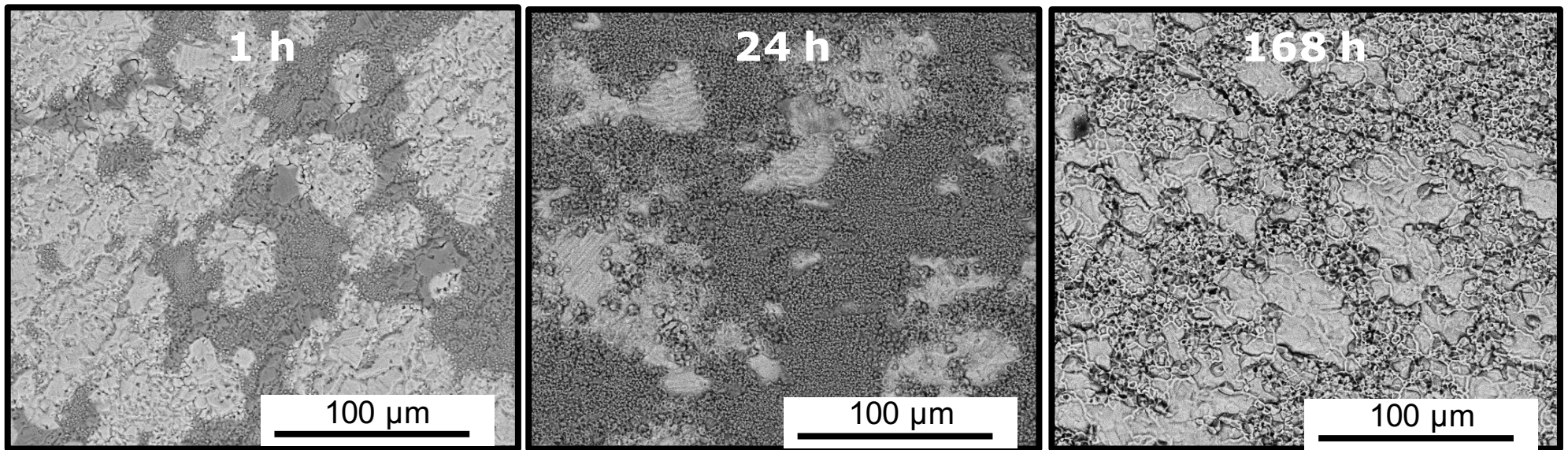




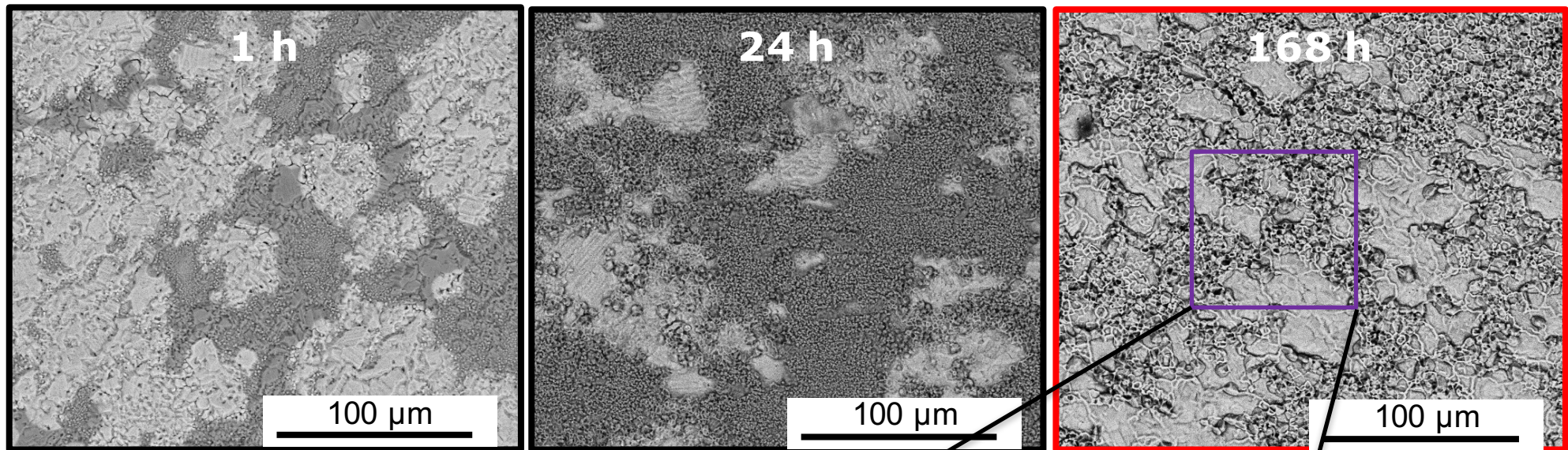
Absolute humidity



- Similar oxidation rate up to 20 % H₂O
- Rapid initial oxidation of 441 at 40 % H₂O
- Humidity more important than pO₂

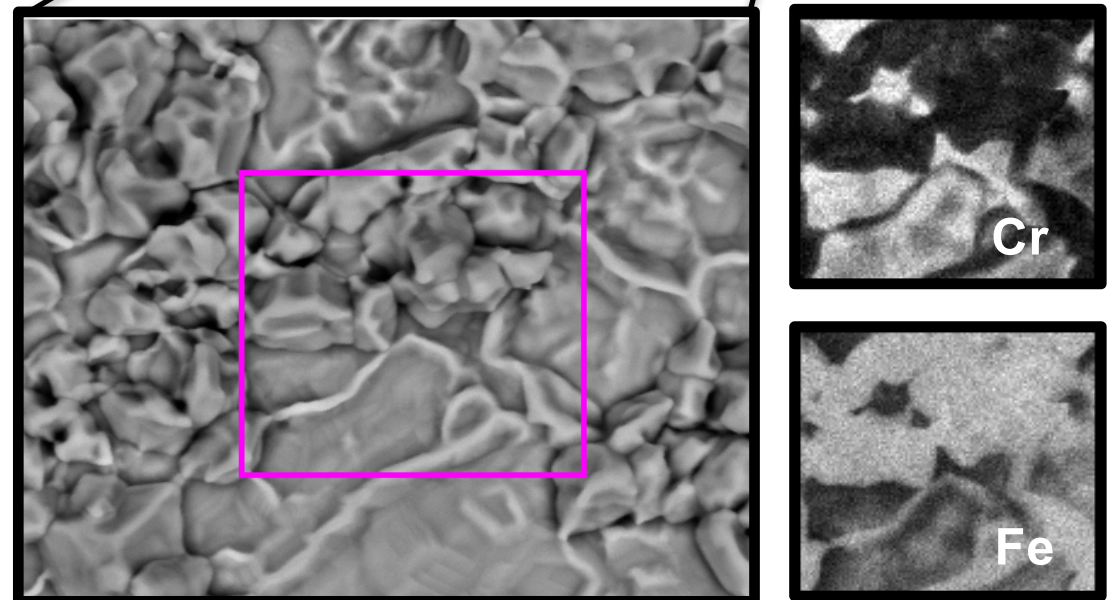


AISI 441



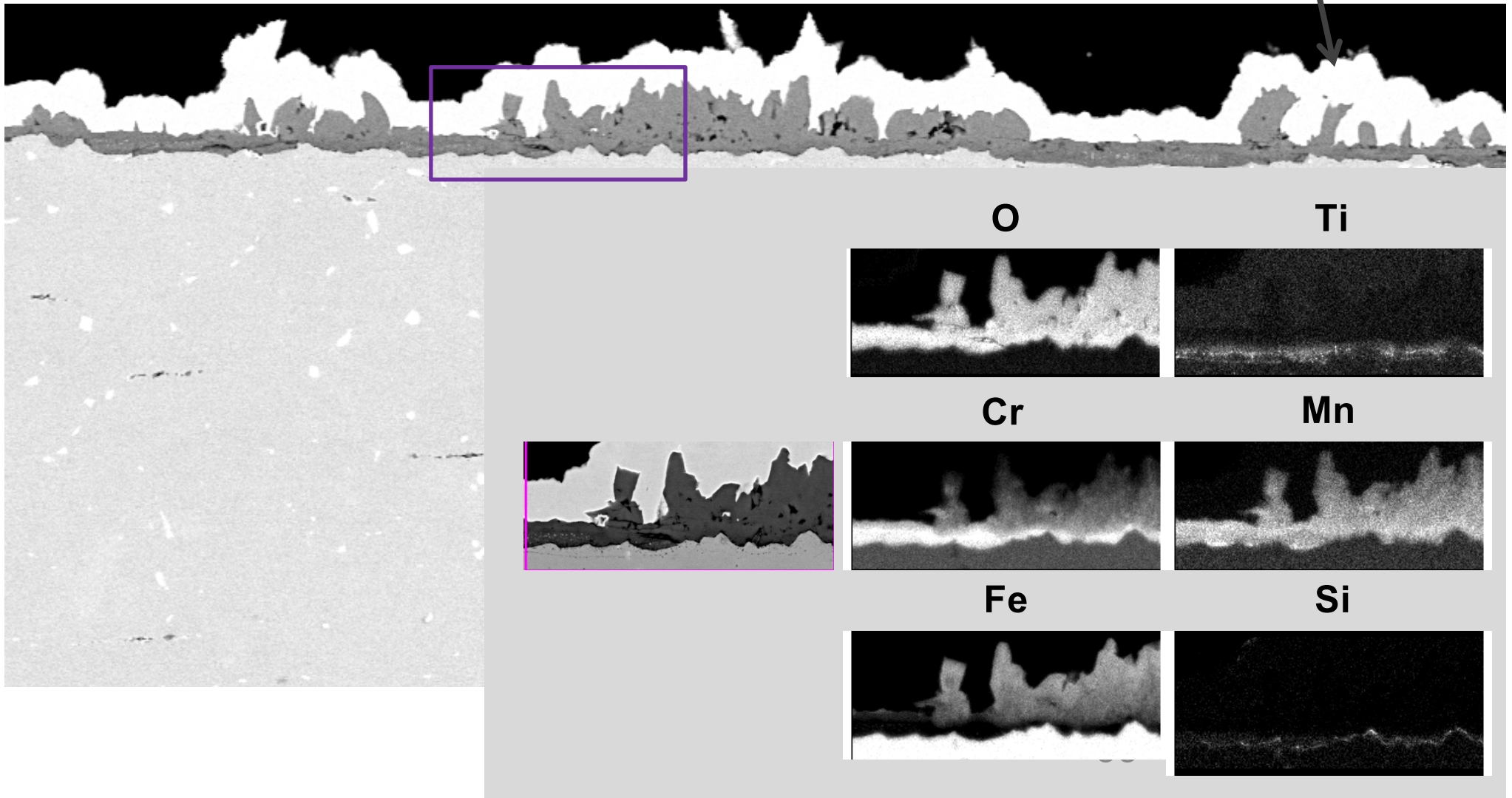
AISI 441

- Iron oxide competing reaction – fast oxidation

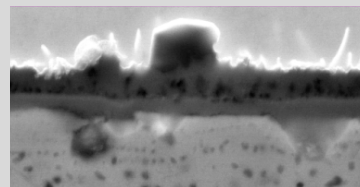
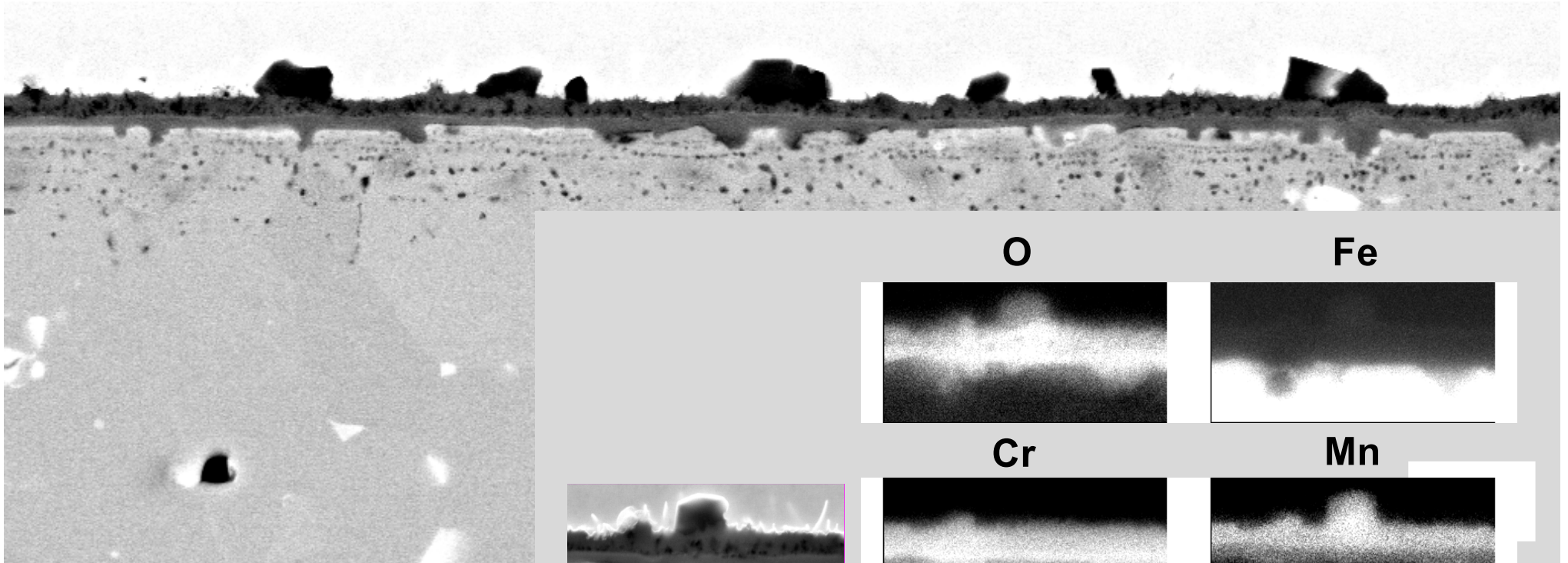


AISI 441 - 500 h

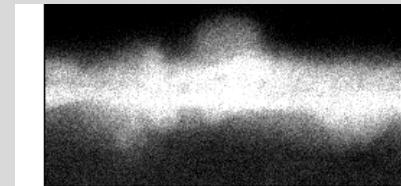
Ni – sample prep.



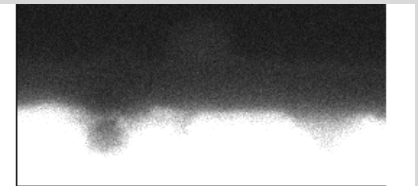
AISI 441 Ce - 168 h



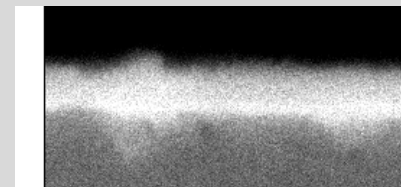
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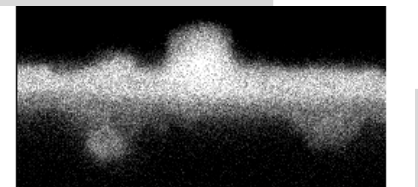
Fe



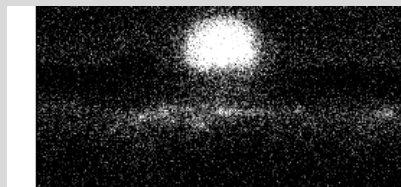
Cr



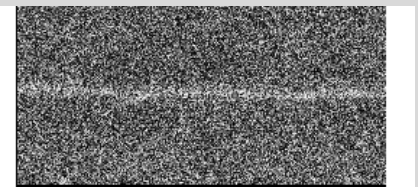
Mn



Si



Ce

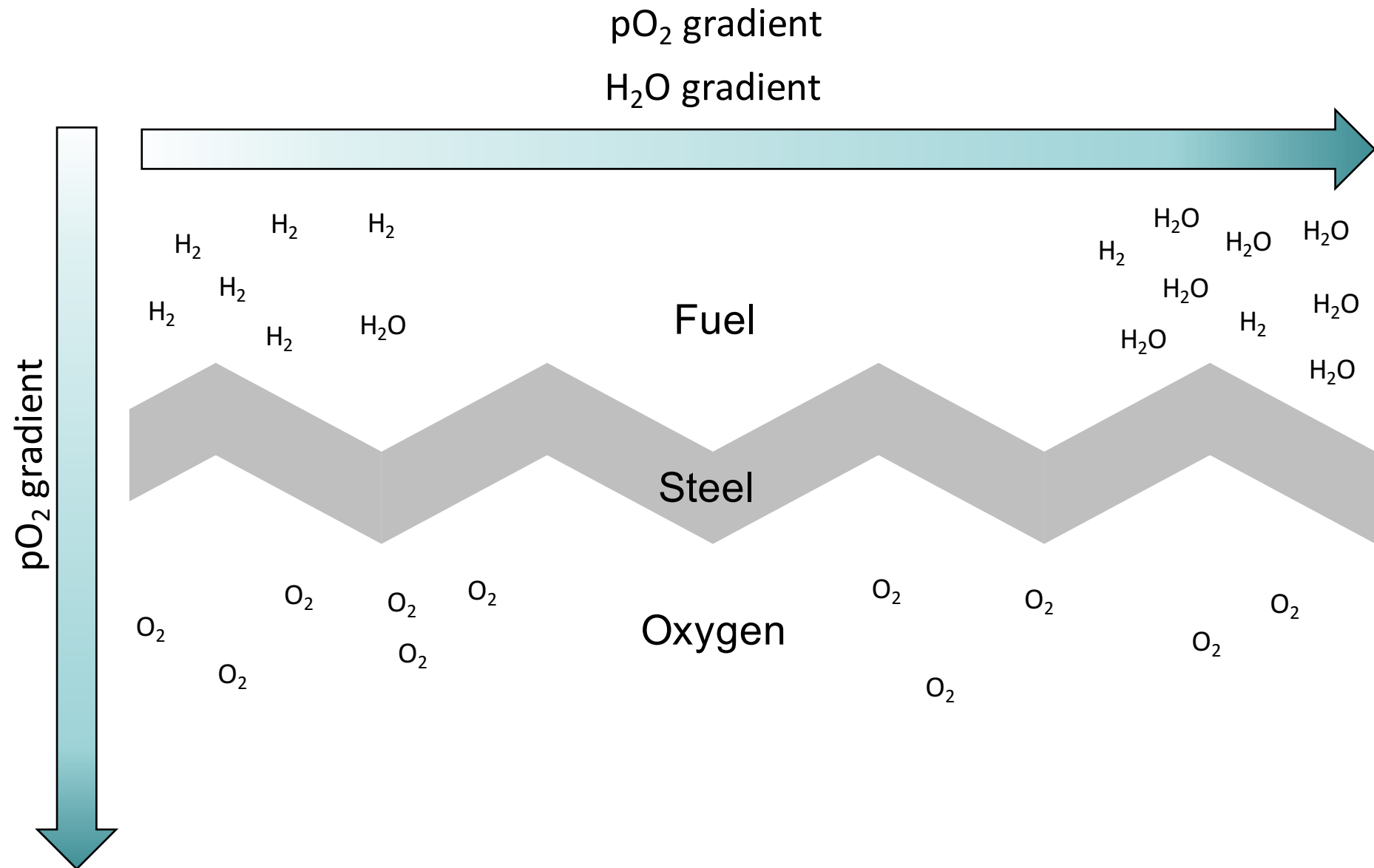


Dual atmosphere

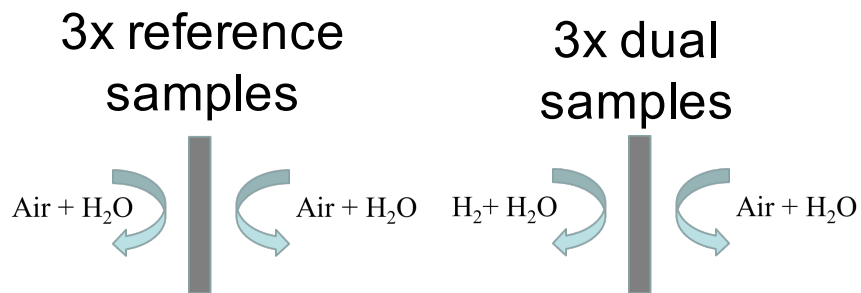
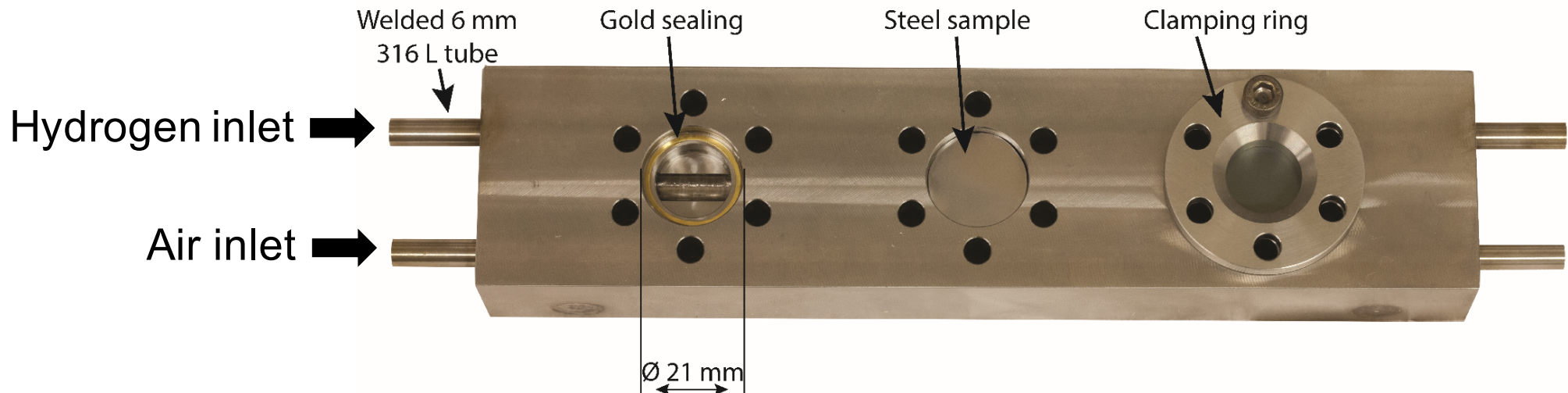
Do ferritic steels corrode differently in a dual atmosphere?

Motivation:

- Closer to reality exposure
- Reduced SOFC operating temperature



Experimental



- Pre-oxidation 3 h at 800 °C
- 1000 h exposure (up to 3000 h)
- 600 °C
- High flow rate air + 3 % H₂O

Material	Fe	Cr	C	Mn	Si	W/Mo	Nb	Ti	RE
AISI 441	Bal.	17.8	0.012	0.26	0.55	no	0.48	0.14	no

Visual inspection of air sides

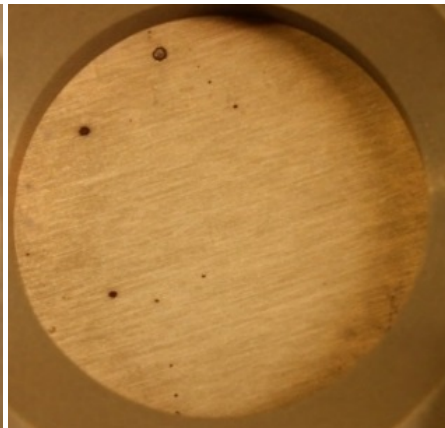
Single
atmosphere

600 °C

Dual
atmosphere



1000 h



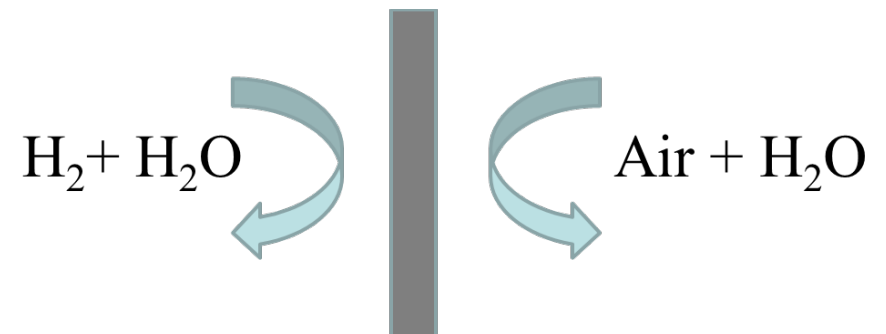
3000 h



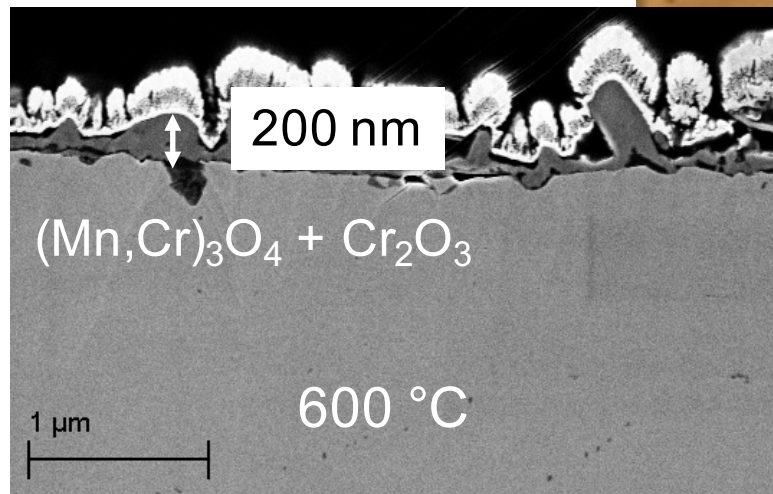
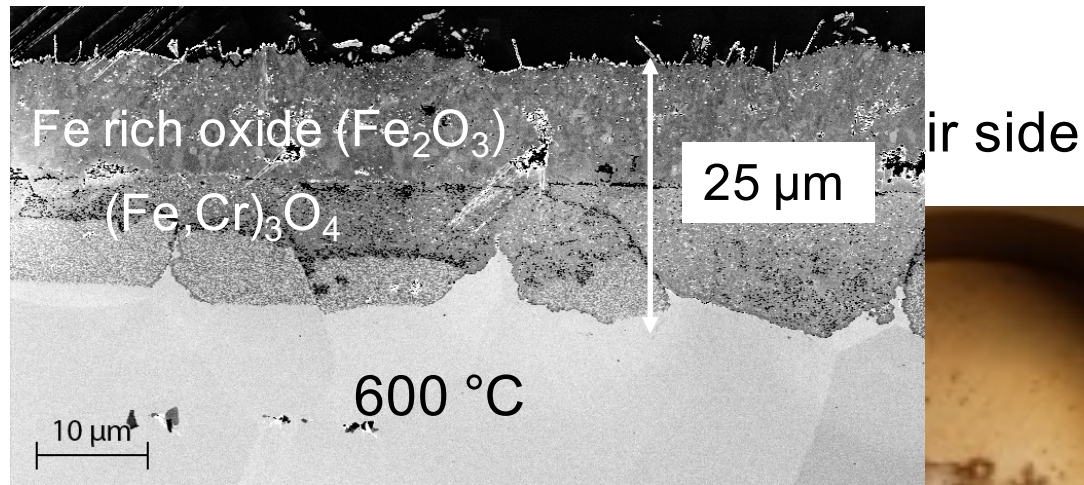
1000 h



3000 h

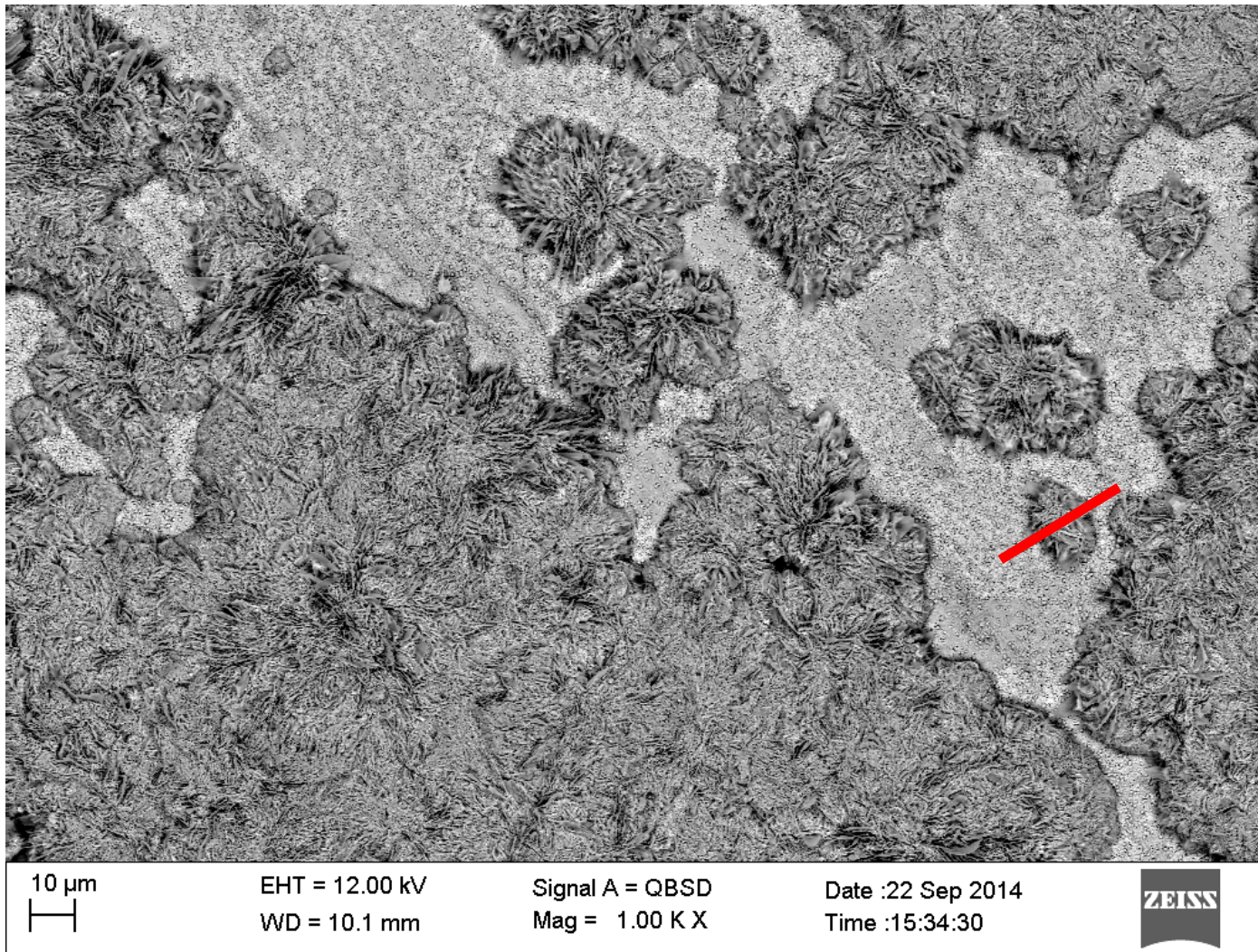


Oxide scale morphology

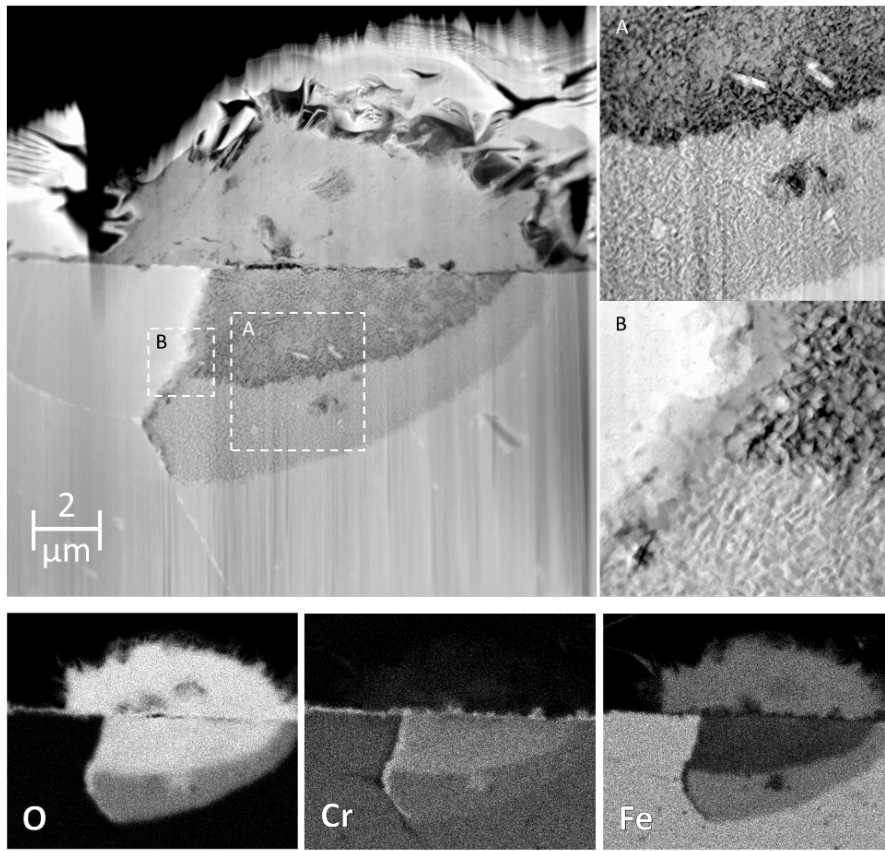


600 °C early oxidation

Surface of air side 1000 h



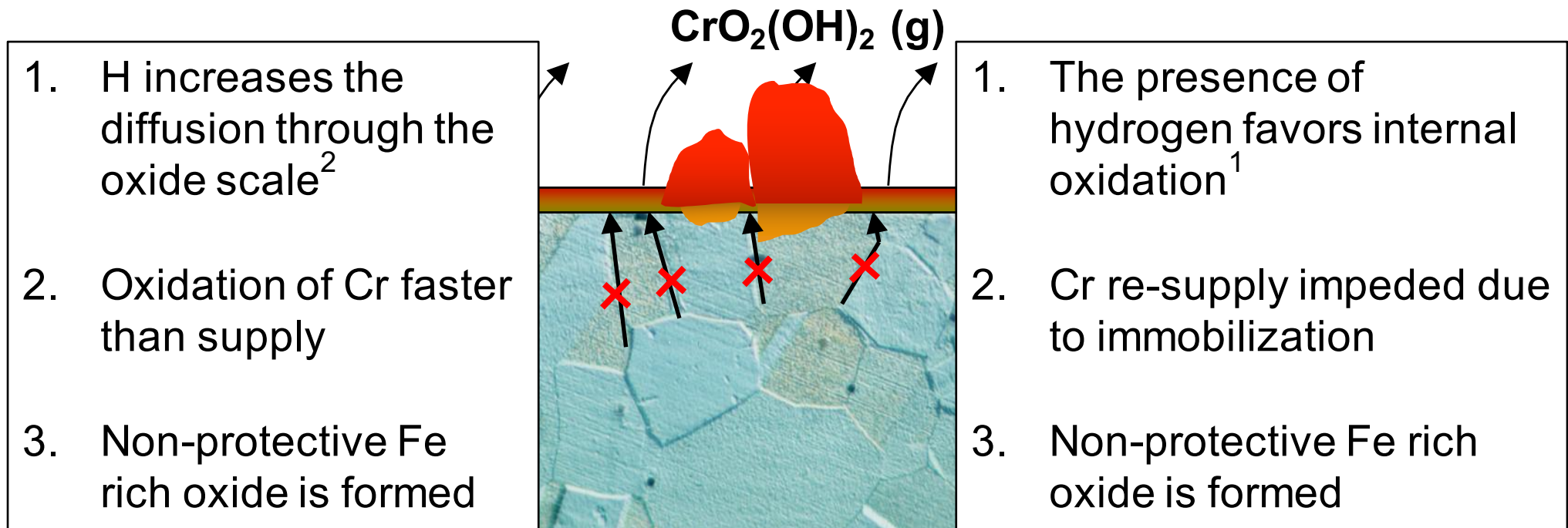
Initiation of breakaway



- Outward growing hematite Fe_2O_3
- Inward growing spinel $(\text{Fe,Cr})_3\text{O}_4$
- Inner reaction zone, miscibility gap Fe-Cr-O
- Remnants of initial Cr_2O_3
- Enrichment of Cr in alloy grain boundary

600 °C, dual atm, 1000 h

Mechanism for H induced breakaway



Condition to maintain
a protective scale:

$$n_{\text{Cr}}(\text{Oxidation}) + n_{\text{Cr}}(\text{Evaporation}) < n_{\text{Cr}}(\text{Re-supply})$$

CO/CO₂

- Crofer APU 0.3 mm
- 700 ° C
- 50/50 CO/CO₂ (200 ml/min each)
- Discontinuous exposure
- Three sets of samples:
 - Uncoated
 - Preoxidized in air 24 h 800 ° C
 - 10 nm Ce coated



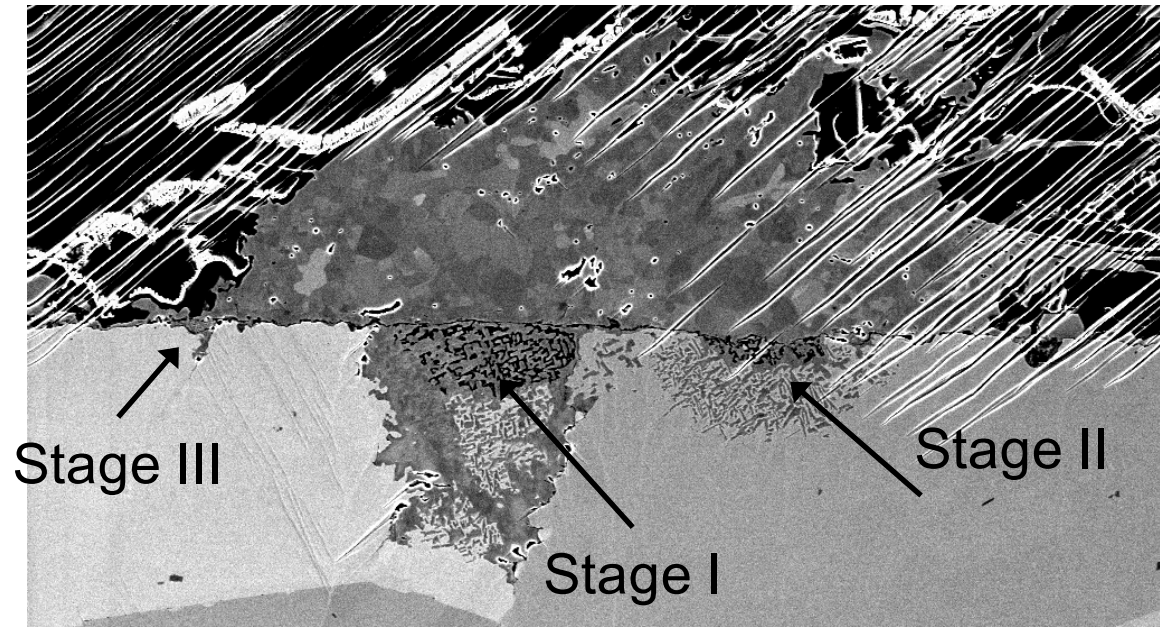
T	700	750	800
CO/CO2	30/70	30/70	30/70
CO/CO2	40/60	40/60	40/60
CO/CO2	50/50	50/50	50/50

Summary

- PVD coatings
 - Reduce corrosion
 - Reduce chromium evaporation
 - Reduce electrical resistance
- Self-healing of pre-coated interconnects
- New challenges
 - High humidity
 - Dual atmosphere effect
 - CO containing atmospheres

extras

Propagation

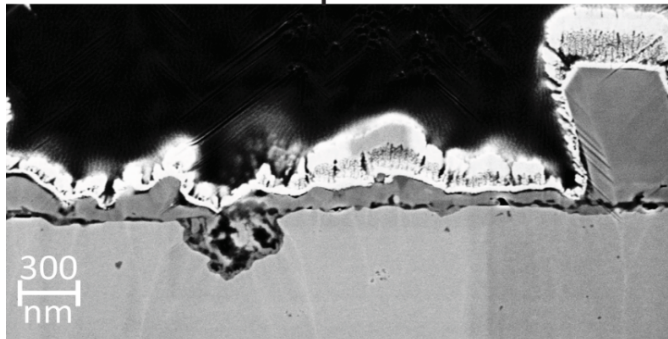


Dual atm, 600 °C, 1000 h

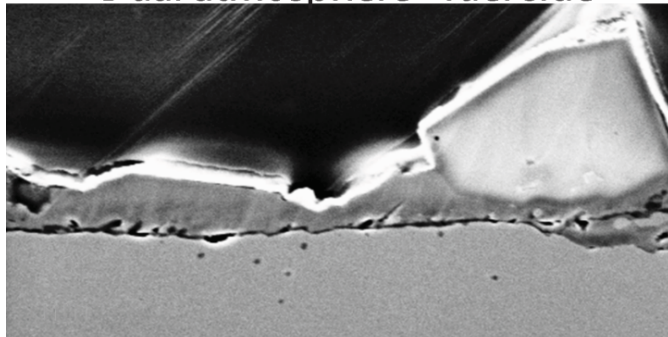
Fe rich crater spills over to neighbouring oxide scale and dilutes the Cr rich protective oxide.

Protective scales

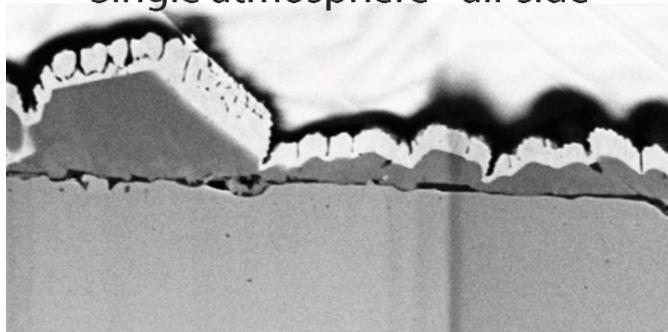
Dual atmosphere - air side



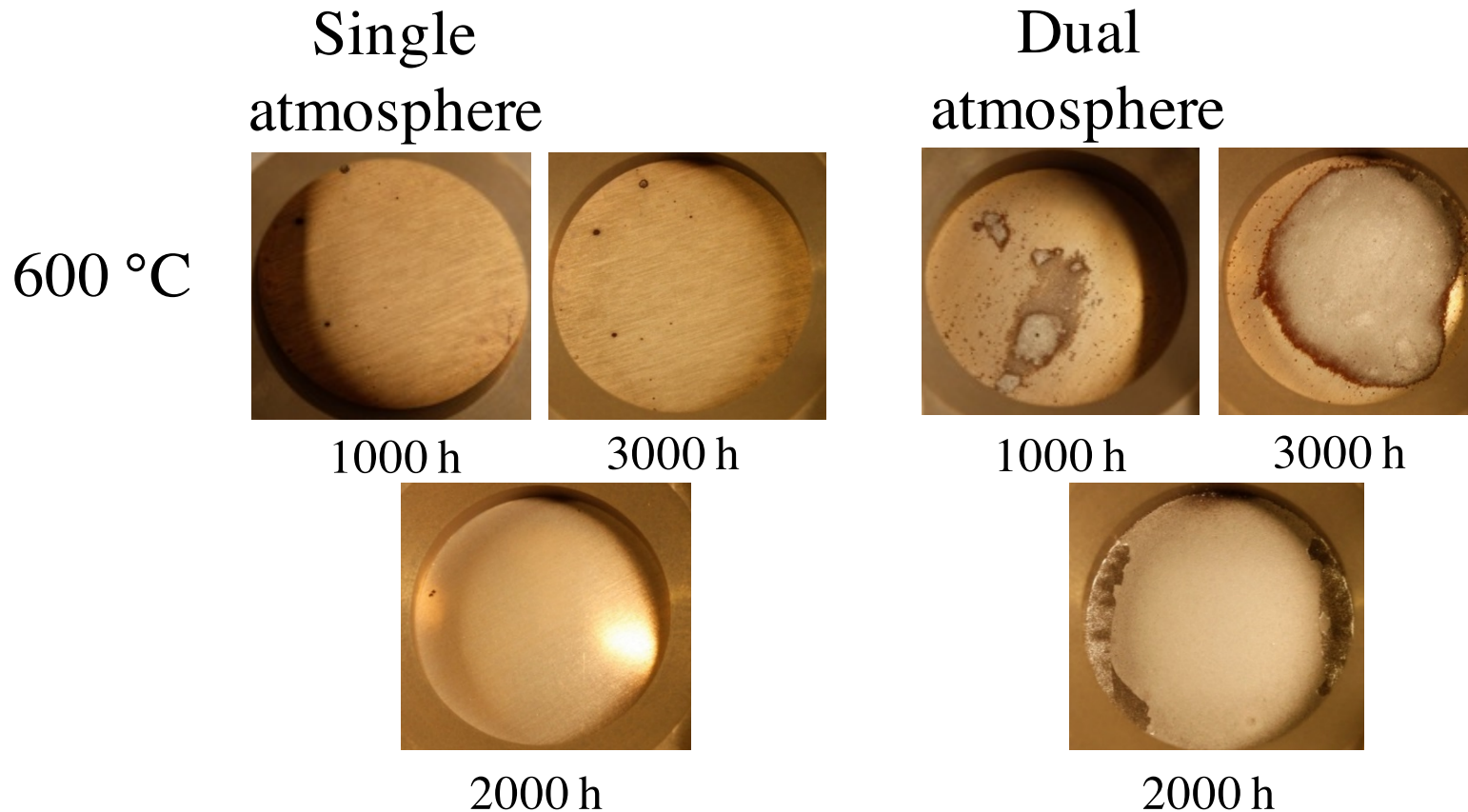
Dual atmosphere - fuel side



Single atmosphere - air side



Preoxidation



- Even more severe for non-preoxidized samples